# Monitoring of I-235 Pedestrian Bridges



Presentation to University of Iowa Civil Engineering Students

September 29, 2005





#### **Bridge Location & I-235 Corridor**

# I-235 Reconstruction

### 70 Bridges reconstructed or replaced

### \$400 million total construction cost Pedestrian Bridges

- <sup>1st</sup> bridge completed January 2004
- Two similar bridges constructed 2005



# Gateway to the City of Des Moines



- Gateway to the City
- Arch spans ranging from 70 m to 80 m
  - 80 m @ Botanical (88.5 m total bridge)
  - ♦ 80 m @ 40<sup>th</sup> Street (83.2 m total bridge)
  - ♦ 70 m @ 44<sup>th</sup> Street (78.5 m total bridge)

- Gateway to the City
- Spans ranging from 70 m to 80 m
- Drilled shafts and pile foundations
  - 4 1680 mm drilled shafts @ Botanical
  - ♦ 67 HP 310x79 piles @ 40<sup>th</sup> Street
  - ♦ 78 HP 310x79 piles @ 44<sup>th</sup> Street

- Gateway to the City
- Spans ranging from 74 m to 80 m
- Drilled shafts and pile foundations
- Steel box arch ribs
  - ♦ 500 mm x 700 mm at crown
  - 750 mm x 1250 mm at base





- Gateway to the City
- Spans ranging from 74 m to 80 m
- Drilled shafts and pile foundations
- Steel box arch ribs
- Precast/post-tensioned deck segments





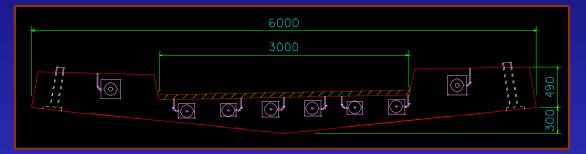
- Gateway to the City
- Spans ranging from 74 m to 80 m
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- Precast/post-tensioned deck segments
- Dywidag hangers





#### **Quick Facts - precast deck panels**

- 6.0 m width x 4.2 m length
- 3.0 m wide walking surface







## **Safety**

### Higher guardrails over traffic area





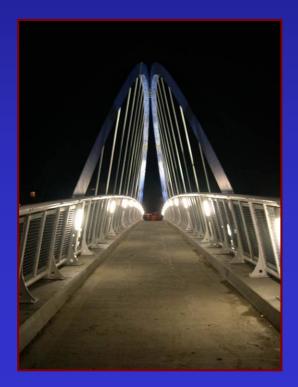
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- > Higher guardrails over traffic area
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- Well-lit at night

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#### **Safety:**

- Higher guardrails over traffic area
- Open environment no hidden corners
- Well-lit at night
- Minimize temptation of vandalism

#### **Comfort**

Vibration from wind and vehicular traffic

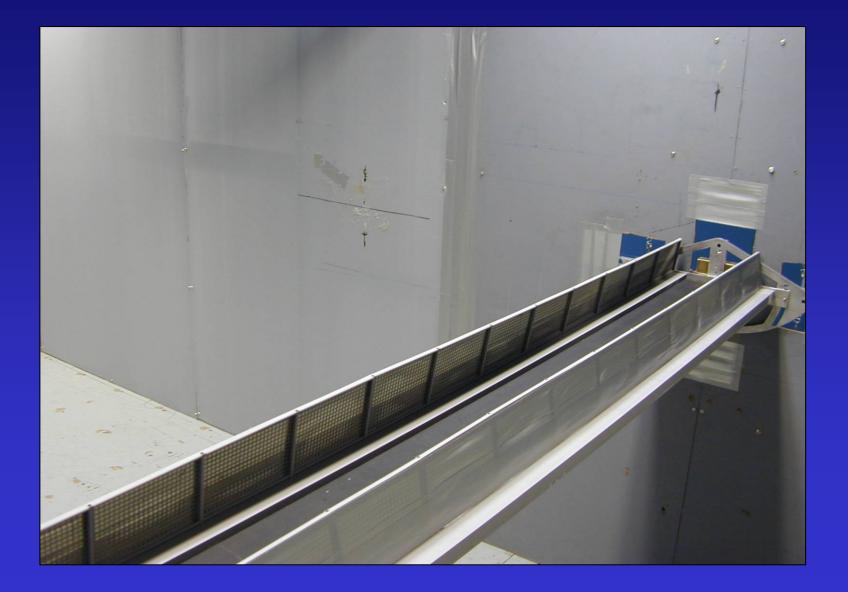
# **Pedestrian Concerns – RWDI Studies**

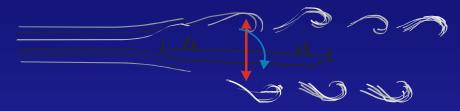


# **Pedestrian Concerns – RWDI Studies**

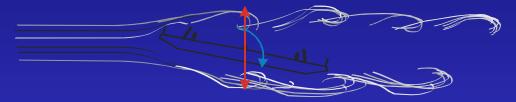


# **Pedestrian Concerns – RWDI Studies**

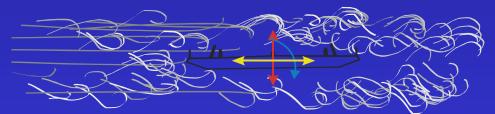




**Vortex-Induced Oscillations** 



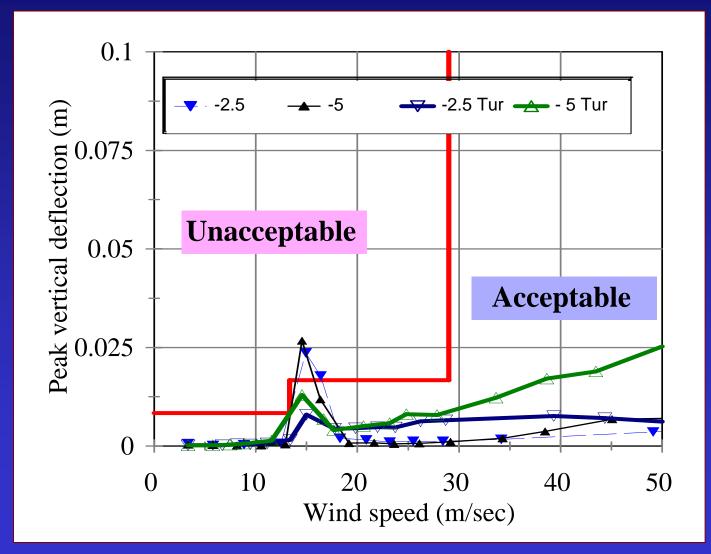
Flutter



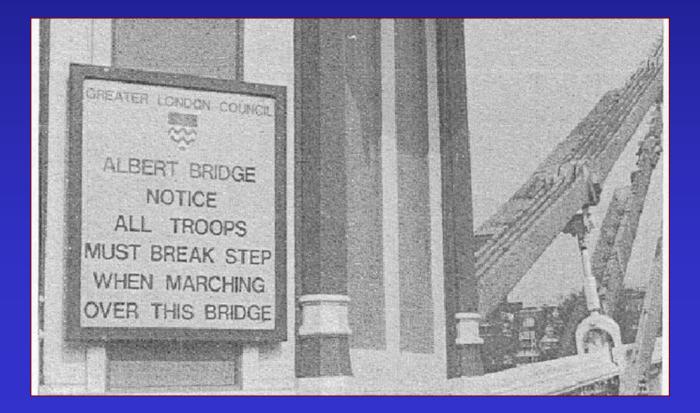
**Turbulence-Induced Buffeting** 

Wind-Induced Instability and Response Phenomena of Bridge Decks

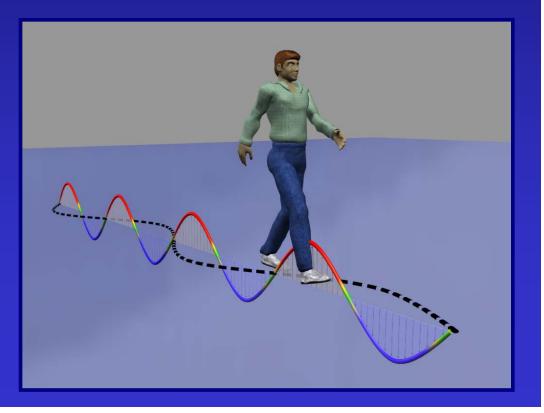
Rowan Williams Davies & Irwin Inc., 650 Woodlawn Road West, Guelph, Ontario, CANADA N1K 1B8 tel: (519) 823-1311, fax: (519) 823-1316, e-mail: sts@rwdi.com



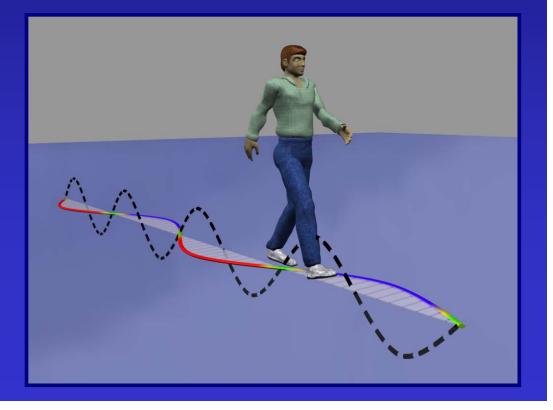
- Vibration from wind and vehicular traffic
- Vibration from pedestrian traffic



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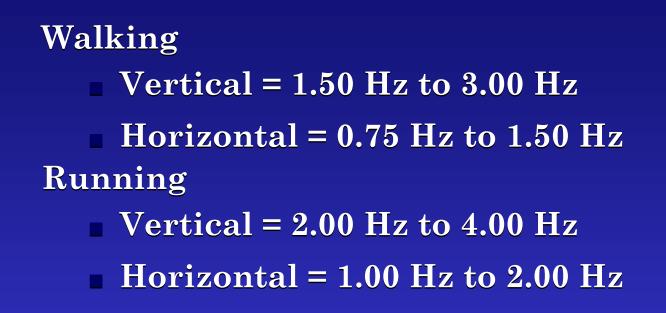


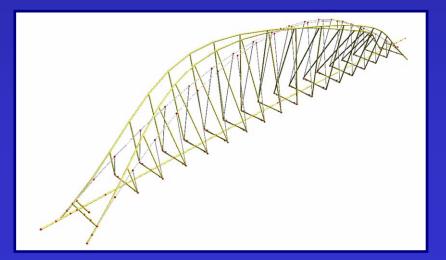
- Vibration from wind and vehicular traffic
- Vibration from pedestrian traffic
- ♦ Lateral sway

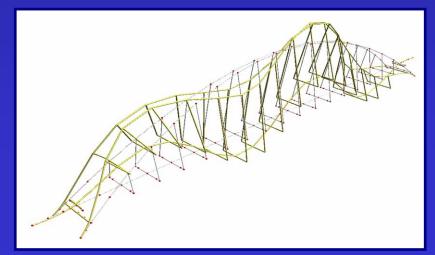


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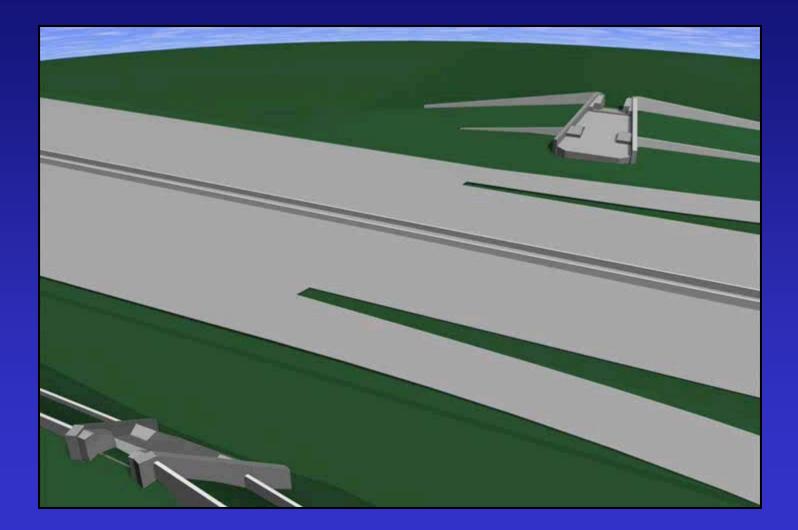








#### **Construction Animation**



# **Steel Erection**





# **Steel Erection**





### **Self-Consolidating Concrete**

Admixtures provide <u>temporary</u> flowability
Measure "spread" rather than "slump"



# **SCC – Formwork is Critical**







# **Precast Deck Panels**







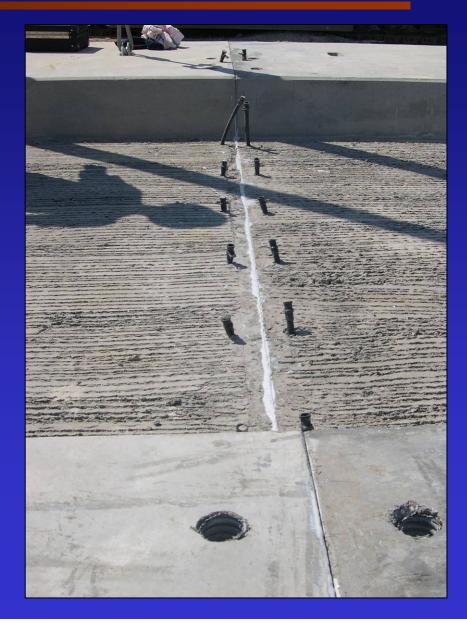
## **Precast Deck Panels – Match casting**



## **Center Panels Stressed on the Ground**







# Hanger and Precast Panel Installation





# **Post-tensioning of Deck Panels**



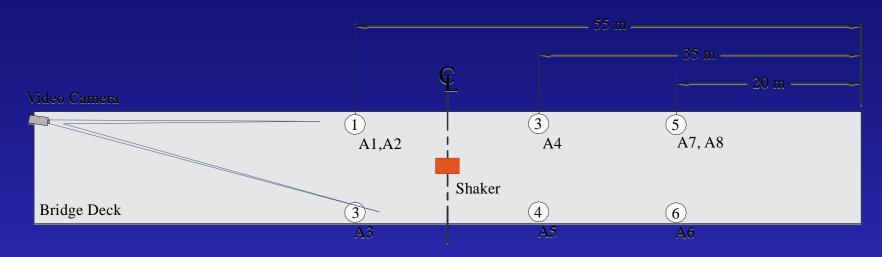
# **Measure Elongation During PT stressing**



# **Aesthetic Lighting**



## **Field Testing of I-235 Pedestrian Bridge**





A1, 3, 4, 5, 6, 7 - Vertical Accelerometers A2&8 - Lateral Accelerometers

True North

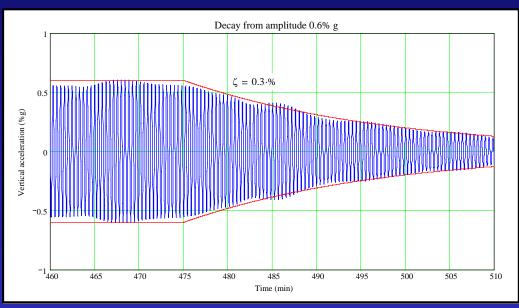
## **Pedestrian Concerns**

# Field testing of Botanical Bridge Mechanical shaker



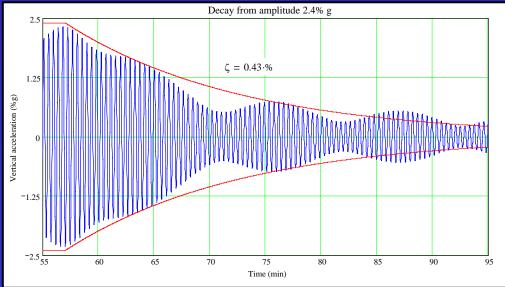


## **Identification of Structural Damping**



#### Test 8 forced excitation at 2.344 Hz

Test 26 forced excitation at 2.344 Hz plus 5 jumping individuals



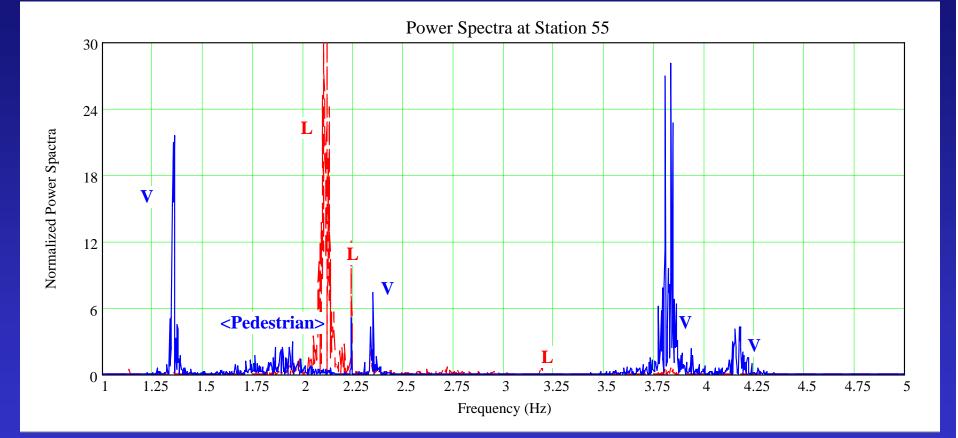
## **Pedestrian Concerns**

Field testing of Botanical Bridge
 Mechanical shaker
 Human response





## **Identification of Modes**



Power spectra from walking of 33 individuals Test 35 - low pass filtered at 20 Hz

## **Concrete Panel Cracking**

## Minor cracking of panels occurred during 2003 construction





#### **Construction Monitoring – 2005**

Unequal loading of hanger rods considered most likely cause of panel cracking

ISU Bridge Engineering Center hired to perform monitoring during construction of 2005 bridges

**Goals of monitoring:** 

- Short term eliminate panel overstresses during construction
- Long term monitor redistribution of loads in hangers (concrete creep)

#### **Instrumentation and Monitoring**

Fiber optic sensors (FOS) can be used to monitor:

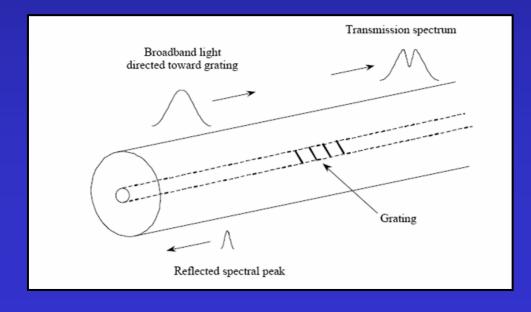
- **Temperature**
- Moisture/humidity
- Pressure
- Strain

ISU Bridge Engineering Center has used FOS for a number of projects over past few years

## **Fiber Optic Strain Sensors**

## Fiber Bragg Gratings (FBG)

- Introduced 1995
- FBG reflects very narrow band of wavelengths – all others pass through
- Any change in strain/temperature causes proportional shift in reflected spectrum

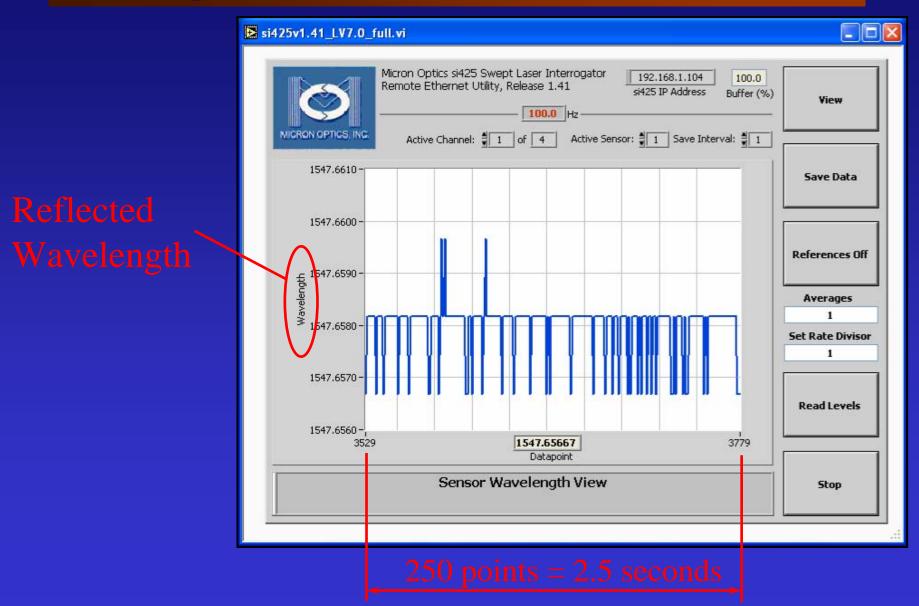


#### **Fiber Optic Sensors**

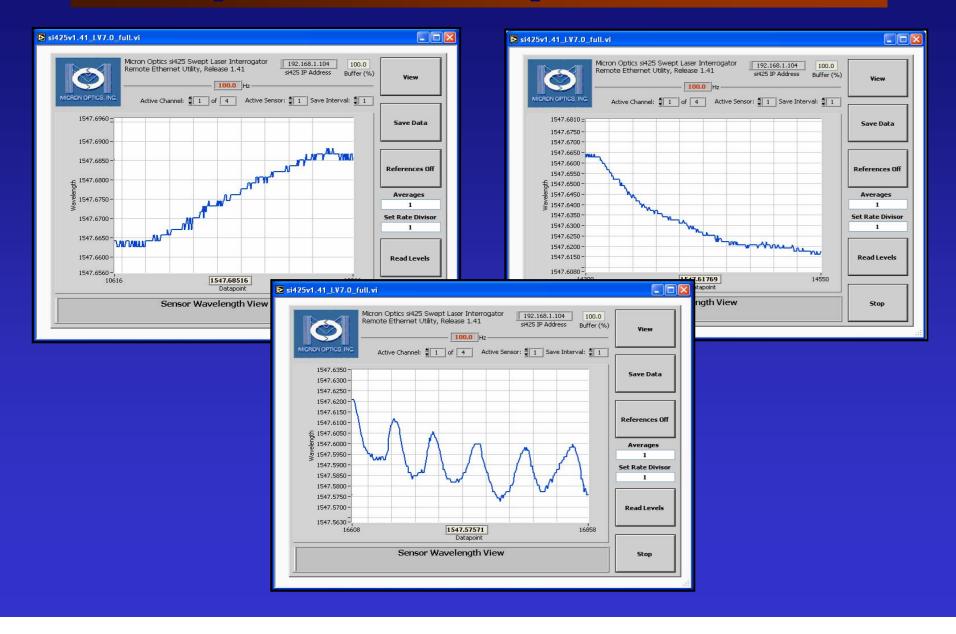
## Advantages:

- No drift during long term monitoring
- Very durable when embedded or installed on completed structure
- Low signal loss with long lead lengths.
- Can be serially multiplexed
- **Disadvantages:**
- Expensive compared to convention strain sensors
- Delicate and easily damaged during construction

#### Fiber Optic Strain Sensor – data collected



### Fiber Optic Sensors – sample data collected



## **Fiber Optic Sensors - Installation**







## Fiber Optic Sensors – Handling in Field





#### **Problems with FOS survivability**

## **Original intent of monitoring:**

- Connect sensors in series to simultaneously read multiple  $\lambda$
- Each quadrant of bridge separated
- Monitor load in each hanger as each subsequent panel installed

Damage during construction prevented series connections and required individual readings at each stage

## **Fiber Optic Sensors - Protection**





## Survivability of Fiber Optic Sensors

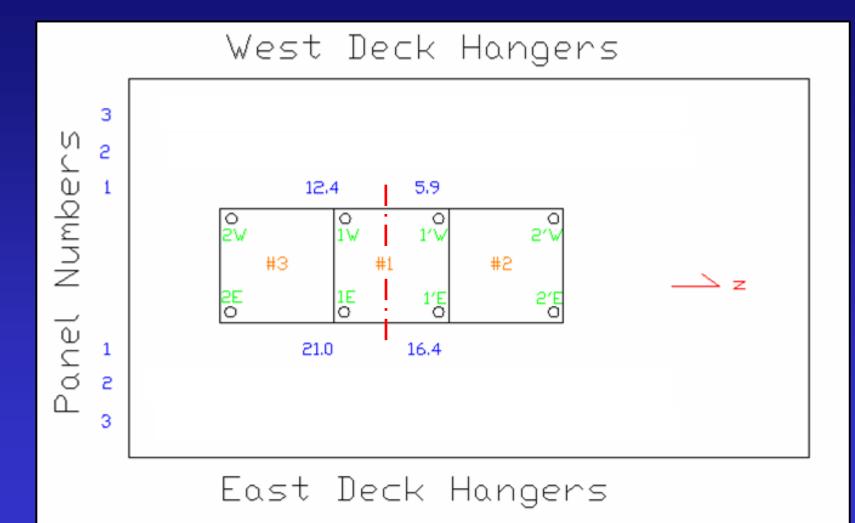
## First bridge – 44<sup>th</sup> Street:

- Total of 28 hangers installed
- Only 13 were usable after construction

## Second bridge – 44<sup>th</sup> Street:

- Total of 36 hangers installed
- Total of 31 hangers working after construction

## **Fiber Optic Strain Sensor Results**



## Long term monitoring of hanger loads



## Natural frequency monitoring - hanger loads

Hanger assumed to be uniform beam subjected to axial load with:

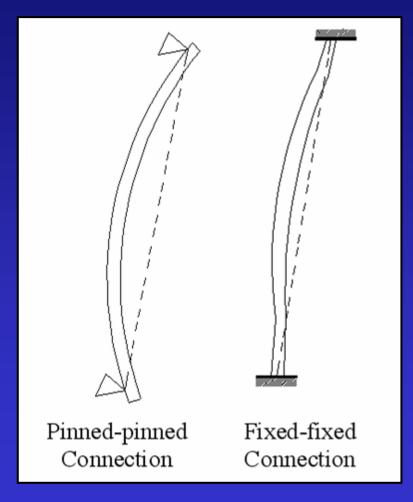
- Distributed mass and elasticity properties
- Length, L
- Area, A
- Flexural rigidity, EI
- Mass density,  $\rho$

$$T = \rho A \left( \frac{L}{n\pi} \left[ \omega_n - \left(\beta_n L\right)^2 \sqrt{\frac{EI}{\rho A L^4}} \right] \right)^2$$

#### **Other Modeling Considerations**

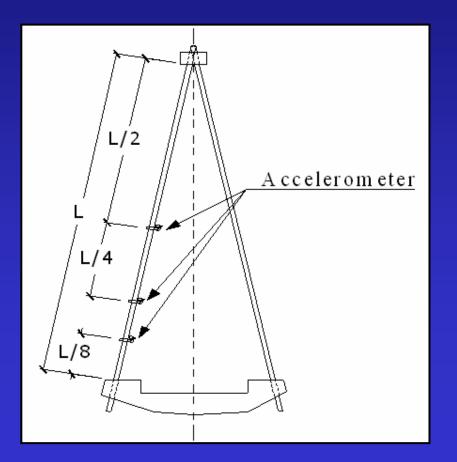
Which section properties are "correct":
Steel rod alone?
Steel rod with grout?
Grout composite w/ rod?

Natural frequencies for simple span beams, β<sub>1</sub>L: Pinned-pinned = 3.141 Fixed-fixed = 4.730

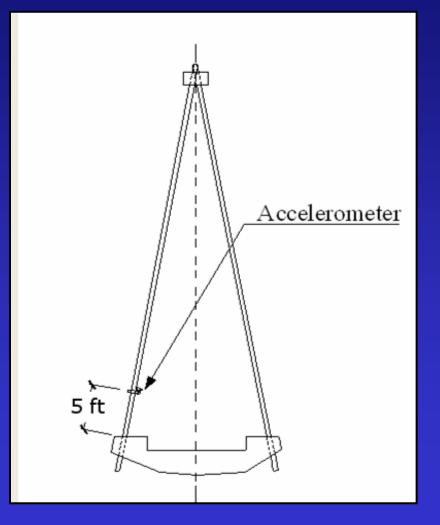


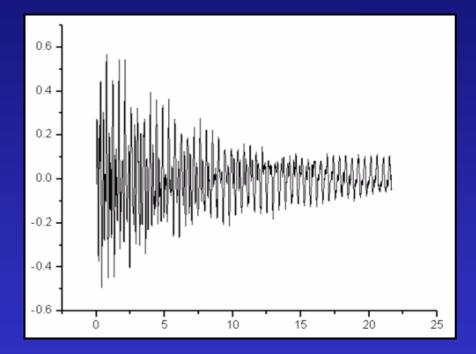
## Vibration Testing of Hanger Rods

Initial testing included varying the position of the accelerometer to ensure identical  $\omega_n$  measured



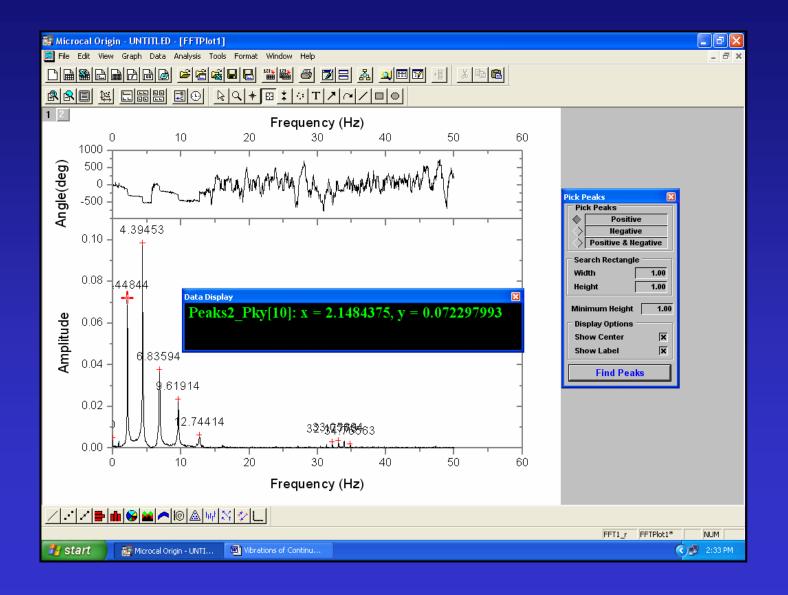
## **Free vibration of hanger rods**





Each hanger excited and allowed to vibrate for 10-15 seconds

#### **Calculation of Natural Frequencies**

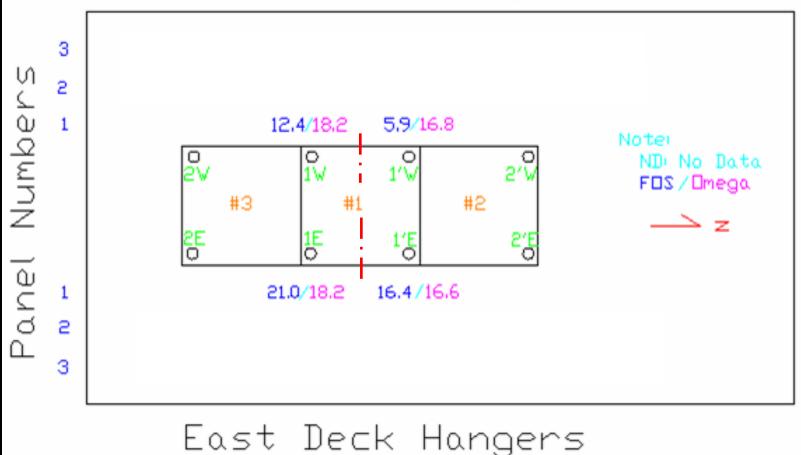


## **Estimated hanger loads – end conditions**

	West Arch		
Hanger	Pinned – Pinned	Fixed – Fixed	Not
	(kips)	(kips)	_ computed
9			<b>r</b>
8	30.8	17.7	
7	31.3	21.9	
6	35.6	27.5	
5	32.5	25.8	
4	33.4	27.4	
3	27.7	22.5	
2	25.6	20.9	
1	36.2	30.7	

## **Comparison of FOS and dynamics results**

## West Deck Hangers



## **Adjustment of Hanger Loads**

Recall that deck must be constructed to match the profile grade as precast

On the shortest hanger rods, a change in length of 1/8" changes force by approx. 40 kips





## **Adjusted Hanger Loads**

	West Arch		
Hanger	Before Adjustment (Pinned-Pinned)	After Adjustment (Pinned-Pinned)	
	(kips)	(kips)	
8	6.0	30.8	
7	27.8	31.3	
6	49.6	35.6	
5	52.3	32.5	
4	33.1	33.4	
3	5.6	27.7	
2	23.2	25.6	
1	83.9	36.2	

#### Conclusions

- Hanger loads are much more uniform than in 2003 bridge construction
- Visual inspection indicates fewer cracks in precast concrete panels
- BEC will return to 2005 bridges in six months to a year to monitor changes in hanger loads due to creep, etc.
- Use of fiber optic strain sensors during construction is difficult due to survivability concerns
- It is possible to use vibration records to monitor loads of axial members which also provide flexural stiffness

## **Questions** ?



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