### Specifications:

Design:
AASHTO LRFD Bridge Design Specifications, 8th Ed., Series of 2017.

### Construction:

Iowa Department of Transportation Standard Specifications for Highway and Bridge Construction, current series, plus applicable General Supplemental Specifications, Developmental Specifications, Supplemental Specifications and Special Provisions

Design Stresses:

Design stresses for the following materials are in accordance with the AASHTO LRFD Bridge Design Specifications, 8th Ed., Series of 2017: Reinforcing steel in accordance with AASHTO LRFD Section 5, Grade 60. Concrete in accordance with AASHTO LRFD Section 5, f'c = 4.0 ksi.

Standards: For details and notes not shown refer to the following Iowa D.O.T Highway Standards:						
Standard	Issued	Revised				
**	?	?				

\*\* Note: "Top Slab Construction Joint Detail" does not apply.

Summary	of Reinforcing S	Steel
Location	Quantity	Total
Headwalls ? Skew	2 @ ?	?
? Barrel Extension		
? Barrel End Section		
5r1 x 3'-6" Dowel Bars		
_		
	Total (LB)	

Concret	Concrete Placement Quantities								
Location	Footing	Walls	Slab	Total					
Headwa <b>ll</b> s ? Skew	2 @	2 @	* 2 @	?					
? Barrel Extension									
? Barrel End Section									
Total (CY)									

<sup>\*</sup> Includes parapet and top of wingwall.

	Design History at This Site (Includes This Design)
Des. No.	Type of Work
X	Х
Χ	Х
Χ	Х
X	Х

PROJECT NUMBER

IOWA DEPARTMENT OF TRANSPORTATION - HIGHWAY DIVISION DESIGN NO.

SHEET NUMBER

Culvert Extension Details ( Sheet 1 of 2 ) Standard Sheet 1043s1 12/29/2020 5:24:52 PM bkloss

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DESIGN SHEET NO. \_\_\_\_ OF \_\_\_ FILE NO.

### General Notes:

It is the intent of this design to extend the existing \_ box culvert.

Electronic copies of original design plans are available to the Contractor as part of the e-files supplied with the contract documents. Dimensions shown on these plans are based on design plans (Original Design No. \_\_\_\_\_).

Faint lines on plans indicate existing structure.

Utility companies and municipalities whose facilities are shown on the plans or known to be within the construction limits shall be notified by the Contractor of the construction starting date.

The R.C.B. culvert extension sections are designed for HL-93 live load and earth fills of \_\_\_\_\_ feet. This design is based on Load and Resistance Factor Design, according to the 2017 AASHTO LRFD Bridge Design Specifications.

Vertical earth pressure, EV=0.120 kcf.

Horizontal earth pressure, EHmax = 0.060 kcf max, EHmin = 0.030 kcf.

The Contractor may submit alternate frost trough dimensions for approval. Any additional costs due to change in the frost trough dimensions is to be paid for by the Contractor.

Floor of barrel is to be finished smooth. Sides of footing are to be formed to

ensure correct line and grade.

The permissible construction joint at the top of the walls may be lowered at the Contractor's option with Engineer's approval.

The vertical bars in the walls may be spliced above the footing at the Contractor's option as follows:

Bar Size Number	4	5	6	7	8	9
Minimum Splice Length	20"	24"	29"	34"	38"	47"

This splice, if used will be at the Contractor's expense

Metal bar chairs spaced at not over 3'-0" C-C In either direction are to be used to support all slab and floor steel as outlined in the Standard Specifications.

The reinforcement supplied for this structure shall be Grade 60. Reinforcing bar

clearances will be as follows:

Edge clearances: 2" except

2¼ to near transverse reinforcing bar Top of floor Bottom of floor 3½ to near transverse reinforcing bar

End clearances:

Vertical top

Vertical bottom 3" or 3½" if overall height of the culvert is not to a full inch

SIGN TO 4

All reinforcing bars and bars noted as dowels supplied for this structure shall be deformed reinforcement unless otherwise noted or shown

Class 20 excavation material unsuitable for backfilling shall be disposed of in a manner that will leave the site in a neat condition.

The price bid for "Removals as Per Plan" shall include the cost for removals of portions of the existing culvert, and the setting of the dowel reinforcing bars into existing concrete.

All dimensions and details shown on these plans pertinent to new construction in relation to existing portions of the structure shall be verified in the field by the

Contractor before starting construction.

The removal of the existing culvert shall be at the front face of the existing parapet. Removals shall be on a vertical plane parallel with the front face of the existing parapet, and to the width of the floor of the proposed extension. The walls shall be cut normal to the barrel walls and as shown on the "Part Removal Plan". The removal line shall be initiated with a 2½"± deep saw cut on the top and both sides of each wall, and across the top of the floor. This saw cut should cut thru any existing longitudinal reinforcing thereby facilitating a neat non-spalled break line. If existing top of parapets will be within 6" of proposed subgrade elevation, the parapets shall be removed down to an elevation 1"± above the top of the existing slab. Any existing parapet vertical bars exposed during parapet removal shall be cut off flush with the parapet removal line and painted with two coats of zinc rich

All removals shall be carefully accomplished and any concrete damaged by the Contractor that is not to be removed shall be repaired by the Contractor at no extra cost to the state. Removals shall be in accordance with Section 2401 of the Standard Specifications.

The proposed culvert extension shall abut against the front face of the existing parapet.  $5z1 \times 2$ -6" dowel reinforcing bars with a 10" minimum embedment into existing concrete shall be set around the entire periphery of the existing culvert. 5z1 dowel reinforcing bars shall be centered in the existing slab, walls and floor. 5z1 dowel reinforcing bars shall be at 1-0" maximum spacing C-C of dowels. 5z1 dowel reinforcing bars shall be set with polymer grout in accordance with Article 2301.03, e, of the Standard Specifications, and current Supplemental Specifications of the Iowa D.O.T. Highway Division.

The roadway will be open to traffic during construction.

Since the highway will not be closed to traffic during this construction, the Contractor may feel temporary shoring (sheet pile or other) is necessary to ensure that the shoulder will not slough in while culvert is being extended. However, if for any reason such shoring is deemed necessary, the Contractor shall submit the shoring plan to the Engineer for approval. Cost of shoring, if required, will be considered incidental to construction and no direct payment will be made. Therefore, all material used for shoring shall remain the property of the Contractor. In addition to the requirements noted above, Article 1107.07, of the Standard Specifications, still applies.

Keyway dimensions shown on the plans are based on nominal dimensions unless stated otherwise. In addition, the bevel used on the keyway shall be limited to a maximum of 10 degrees from vertical.

These bridge plans label all reinforcing steel with English notation (5a1 is

% inch diameter bar). English reinforcing steel received in the field may display the following "Bar Designation". The "Bar Designation" is the stamped impression on the reinforcing bars, and is equivalent to the bar

English Size	3	4	5	6	7	8	9	10	11
Bar Designation	10	13	16	19	22	25	29	32	36

Traffic will be maintained at all times in accordance with the traffic

control plans shown in these plans.

Traffic control adjacent to the culvert will be the responsibility of the Contractor constructing the culvert and is to coordinate construction of the culvert with the Contractor doing the grading.

Any dimensional transition required between existing structure and the extension shall be made in the first \_\_\_\_ of new work.

When de-watering presents a problem for placing the curtain walls as detailed, alternate methods such as steel sheet pile and precast concrete walls may be approved but at no additional cost. The Contractor is to submit to the Engineer for approval complete drawings of the proposed curtain wall alternate before beginning construction.

IOWA DEPARTMENT OF TRANSPORTATION - HIGHWAY DIVISION

DESIGN TEAM

Culvert Extension Details ( Sheet 2 of 2 ) Standard Sheet 1043s2

COUNTY PROJECT NUMBER

### Traffic Control Plan

Note: The roadway will be oper to thru traffic. Refer to the Traffic Control Plan on the road plans in these plans.

### Traffic Control Plan

Note: The roadway will be ope to thru traffic. Refer to the Traffic Control Plan on Design Sheet ??.

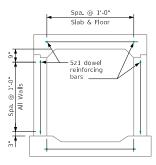
### Traffic Control Plan

Note: The roadway will be closed o thru traffic. Refer to he Traffic Control Plan on the

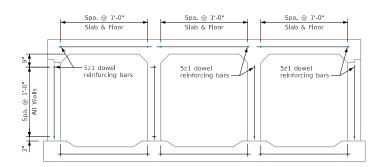
oad plans in these plans.

ote: The roadway will be closo thru traffic. Road closure will be the responsibility of the road Contractor as shown on e road plans.

Traffic Control Plan



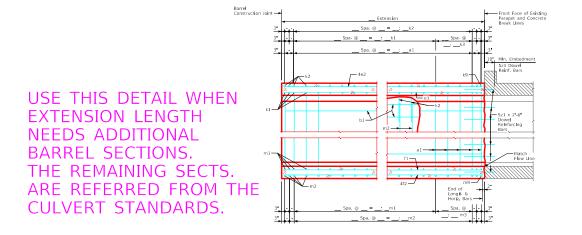
Spa @ 1 0 Slab & Floor reinforcing bars

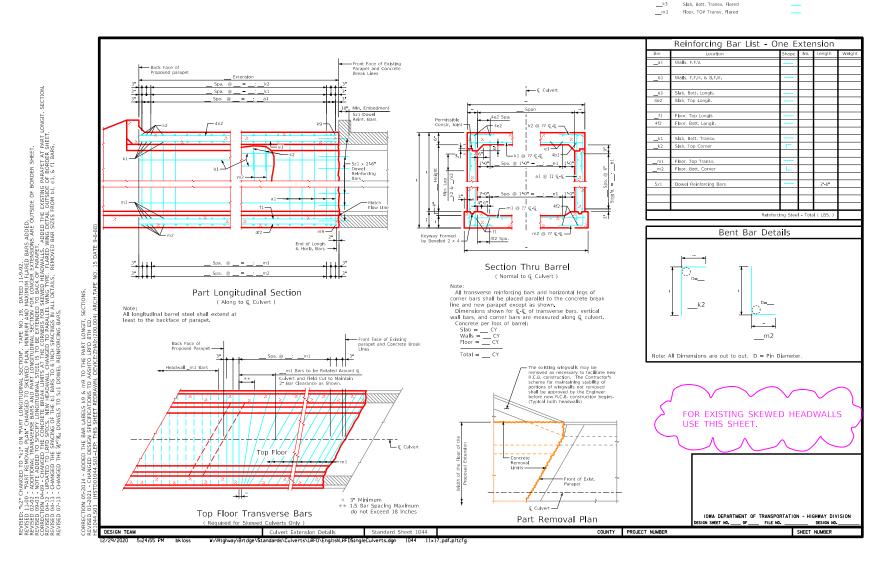


### Section Near Twin Extension ( Showing spacing of 5z1 dowel reinforcing bars

## Section Near Triple Extension

### Section Near Extension ( Showing spacing of 5z1 dowel reinforcing bars )





Proposed Parapet

Headwall m1 Bars

m1 Bars to be Retated Around q

Cilvert and Field Cut to Maintain

2 Bar Glorance as Show

Top Floor

Top Floor

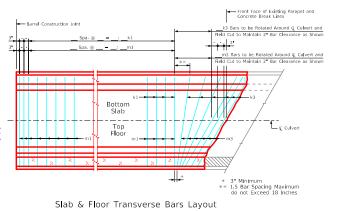
Top Floor Transverse Bars

( Required for Stewed Culverts Only )

FLARED WING EXAMPLE FOR NEW HEADWALL

### FOR EXISTING SKEWED HEADWALLS USE THIS SHEET.

USE THIS DETAIL WHEN EXTENSION LENGTH NEEDS ADDITIONAL BARREL SECTIONS.
THE REMAINING SECTS.
ARE REFERRED FROM THE CULVERT STANDARDS.

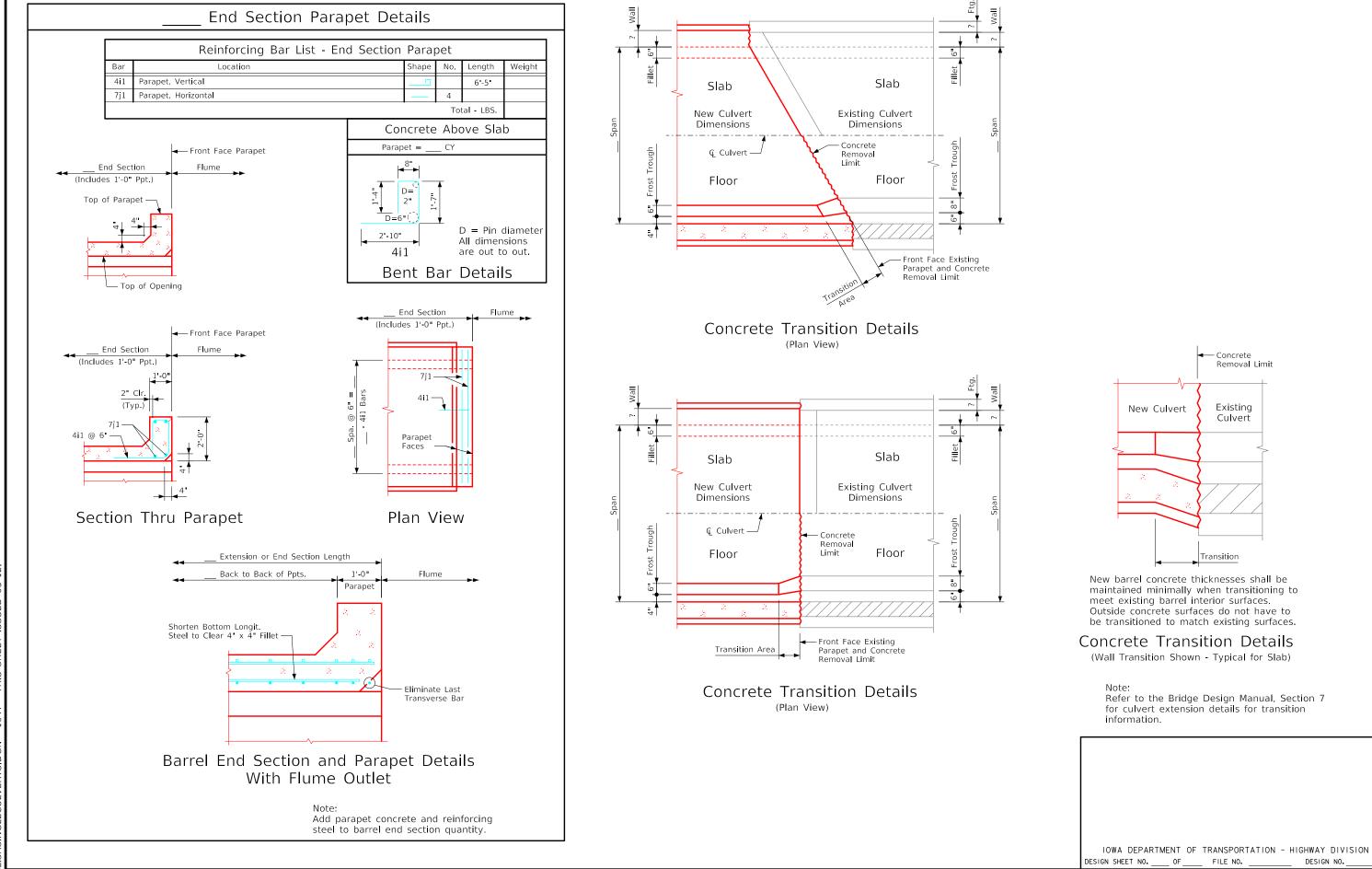


FOR 0° SKEW EXTENSION - PLACE THIS DETAIL ON PLANS

Part Removal Plan



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Standard Sheet 1047

— Concrete Removal Limit

Existing

Culvert

Transition

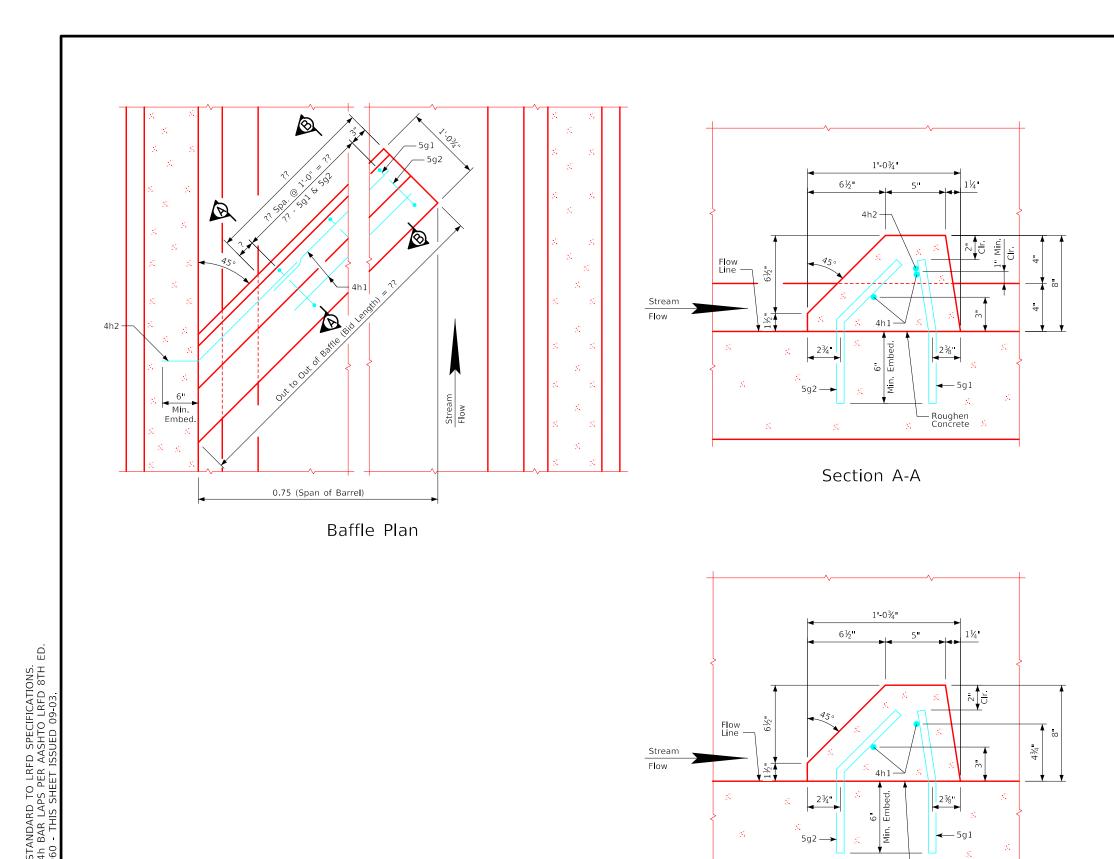
FILE NO.

PROJECT NUMBER

DESIGN NO.

SHEET NUMBER

Culvert Details

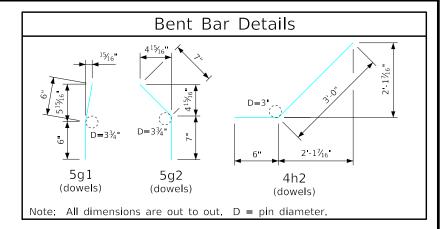


Section B-B

Roughen

COUNTY

PROJECT NUMBER



### Baffle Notes:

- 1. ?? Baffles are to be placed within the reinforced concrete box culvert spaced as shown elsewhere in these plans. Baffles shall be constructed to the dimensions shown on this sheet.
- 2. Clear distance from face of concrete to near reinforcing bar is to be 2" unless otherwise noted or shown.
- 3. All concrete is to be Class C.
- 4. Minimum splice length for the 4h1 and 4h2 bars is 15".
- 5. The 5g1, 5g2 and 4h2 bars shall be set as dowels in drilled holes. Holes are to be 6" deep. The dowels shall be installed in accordance with the manufacturer's recommendations. The dowels shall be installed using a polymer grout system in accordance with Article 2301.03,E, of the Standard Specifications.
- 6. Bonding of the Baffles to the barrel floor shall be in accordance with Article 2403.03,I, of the Standard Specifications.
- 7. The Baffles are to be bid on a linear foot basis. The number of linear feet of Baffle installed will be paid for at the contract price per linear foot for "Baffle or Weir for Reinforced Concrete Box Culvert" based on plan quantity. Price bid for "Baffle or Weir for Reinforced Concrete Box Culvert" shall be full compensation for furnishing all material and all of the equipment and labor required to construct the baffles in accordance with these plans and current Specifications.
- 8. Cross sectional area of the Baffle is 0.53 square feet.

Baffle Quantitie	S	
Item	Unit	Quantity
Baffle for RCB Culvert	L.F.	

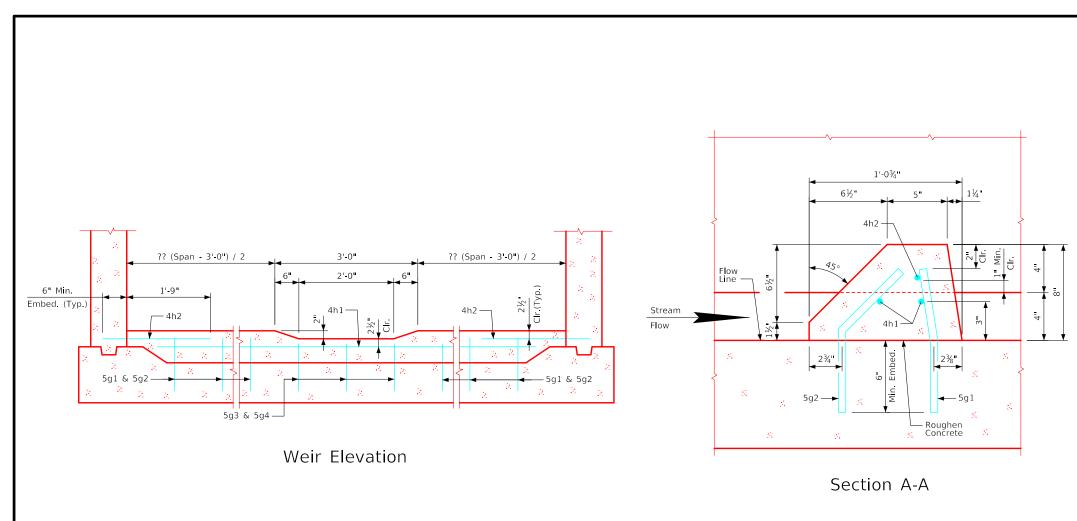
IOWA DEPARTMENT OF TRANSPORTATION - HIGHWAY DIVISION
DESIGN SHEET NO. \_\_\_\_\_ OF \_\_\_\_ FILE NO. \_\_\_\_\_ DESIGN NO. \_\_\_\_\_

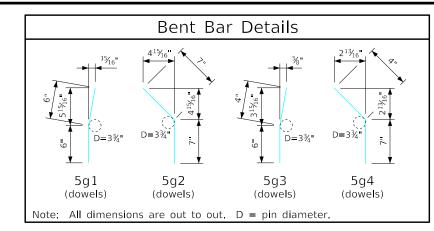
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DESIGN TEAM Culvert Baffle Details Standard Sheet 1060 12/29/2020 5:24:57 PM bkloss W:\Highway\Bridge\Standards\Culverts\LRFD\EnglishLRFDSingleCulverts.dgn 1060 11x17\_pdf.p

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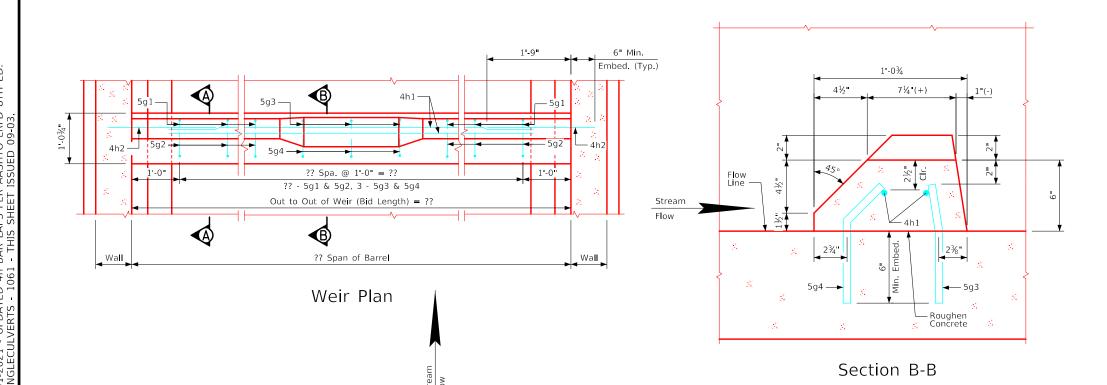


### Weir Notes:

COUNTY

PROJECT NUMBER

- 1. ?? Weirs are to be placed within the reinforced concrete box culvert spaced as shown elsewhere in these plans. Weirs shall be constructed to the dimensions shown on this sheet.
- 2. Clear distance from face of concrete to near reinforcing bar is to be 2" unless otherwise noted or shown.
- 3. All concrete is to be Class C.
- I. Minimum splice length for the 4h1 and 4h2 bars is 15".
- 5. The 5g1, 5g2, 5g3, 5g4 and 4h2 bars shall be set as dowels in drilled holes. Holes are to be 6" deep. The dowels shall be installed in accordance with the manufacturer's recommendations. The dowels shall be installed using a polymer grout system in accordance with Article 2301.03,E, of the Standard Specifications.
- 6. Bonding of the Weirs to the barrel floor shall be in accordance with Article 2403.03,I, of the Standard Specifications.
- 7. If barrel span is less than 6'-0" then 4h2 bars shall be field bent to provide 2" min. clear distance from the top of the notch.
- 8. The Weirs are to be bid on a linear foot basis. The number of linear feet of Weir installed will be paid for at the contract price per linear foot for "Baffle or Weir for Reinforced Concrete Box Culvert" based on plan quantity. Price bid for "Baffle or Weir for Reinforced Concrete Box Culvert" shall be full compensation for furnishing all material and all of the equipment and labor required to construct the Weirs in accordance with these plans and current Specifications.
- 9. Cross sectional area of the Weir is 0.53 square feet.



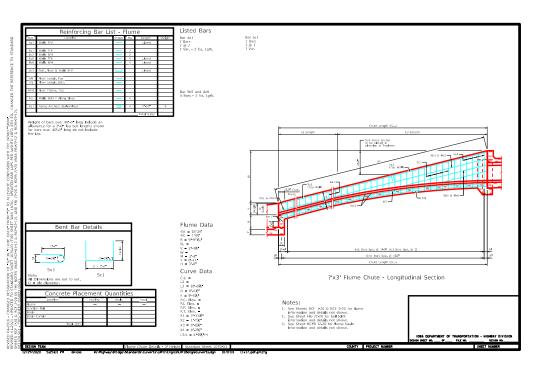
	Weir Quantities	<del></del> 5	
	Item	Unit	Quantity
Weir for R	CB Culvert	L.F.	
	IOWA DEPARTMENT OF TRANSPORT.	ATION - HI	GHWAY DIVISION
	DESIGN SHEET NO OF FILE NO		DESIGN NO

SHEET NUMBER

DESIGN TEAM Culvert Weir Details Standard Sheet 1061

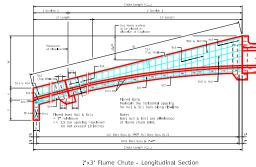
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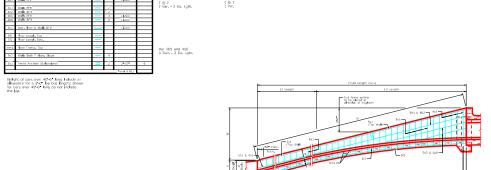
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Bar 5c1 ? Bars ? @ ? ? Var.

?'x3' Flume Chute - Longitudinal Section

Notes:
1. See Sheets RCF 1-20 & RCF 2-20 for
Information and details not shown.

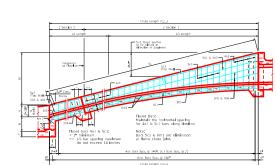
# 3:1 SLOPE FLUME





30.	Location	Shape	Mo	Length	Weight	Bar 4a1
16	Walls FFV	-		Usted		? Bars ? @ ?
61	Wals FFH - Section 1	_	2		-	? Var. 2 Ea. L
th/2	Walls BPH - Section 1		2		-	
153	Wals FFH - Section 2		- 2		_	
154	Walls Birth - Section 2		2		-	
th5	Wals FFH - Section 1	_	4	Distect	-	
bś	Walls B <sup>2</sup> H - Section 1	_	4	Usbed	=	
×:	Bott, Floor & Walls BFV			Listed	$\blacksquare$	
511	Piper Lengit, Top - Section 1	_	-		-	
512	Ficor Longit, Bott, - Section 1	_			-	Bar 5b5 and 4b
513	Floor Longit, Top - Section 2	_			-	4 Bars - 2 Ea. I
551	Floor Longity Botts - Section 2	_			-	
m)	Roor Transv. Top	_			$\blacksquare$	
582	Walls Both F Along Slope - Section 1		-4		-	
54.2	Walls Both F Along Slope - Section 2	_	4		$\blacksquare$	
a1	Fence Anchors (Galversond)		- 2	2.10		

Weight of bars over 40°-0" long include an allowance for a 2°-0" lap but lengths shown for bars over 40°-0" long do not include the lap.

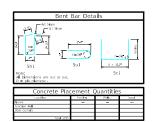


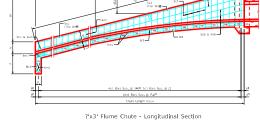
?'x3' Flume Chute - Longitudinal Section

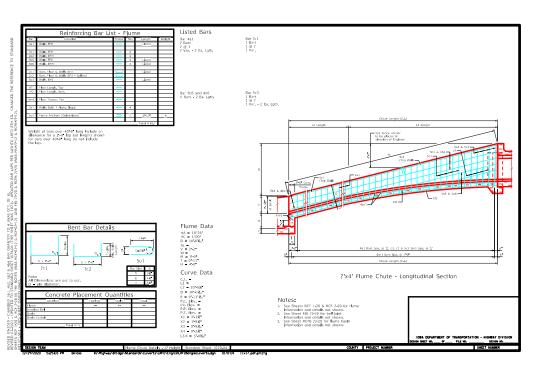
Bent Bar	Details		
Su I  Noto: All Dimensions are out to out. D - pin diameter.	0=30 5+1-2 5c1		
Concrete Pla	cement (	Quantitie:	S
Location	Focong	W015	

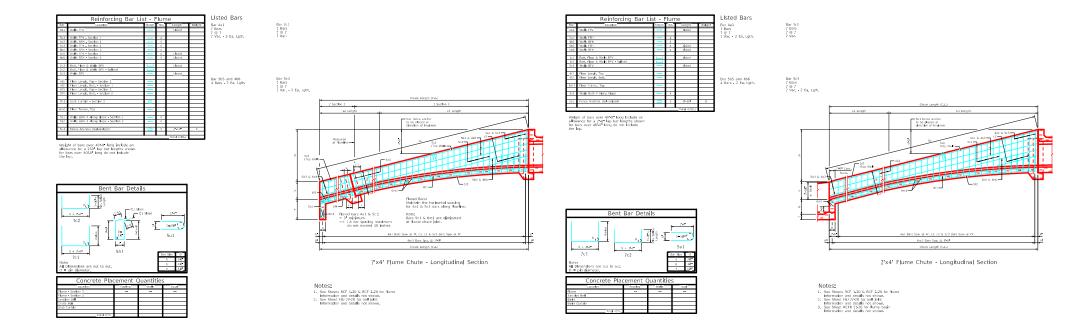
Concrete P	lacement (	Quantitie	S
tocation	Focting	Wals	Total
Rume - Section 1		_	_
Flume - Section 2			
Aunction Bell			
Chute Be			
Basin			
Basin Curtain			
00011-0011011			

# 4:1 SLOPE FLUME

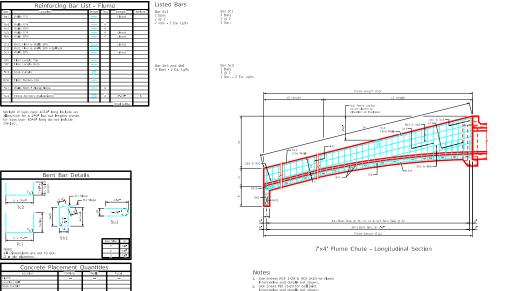


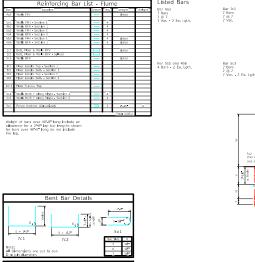


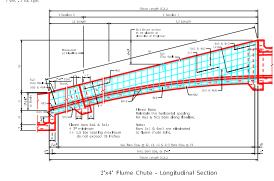




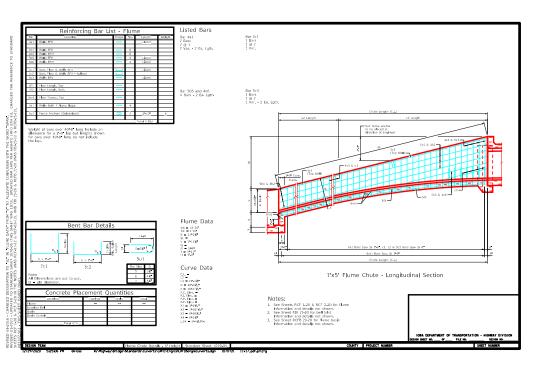


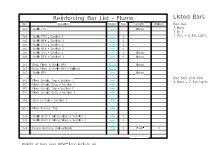






otes: See Sheets RCF 1-20 & RCF 2-20 for flume information and details not shown.





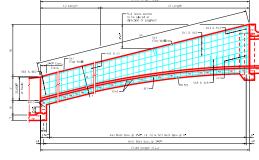












?'x5' Flume Chute - Longitudinal Section

5 x 5	6 x 5	8 x 5	10 x 5	12 x 5	14 x 5	16 x 5
Flume Data  4A = 18929  4C = 19929  4C = 1992  5C = 199	Flume Data  *	Flume Data  44 - 18729  8 - 18729  8 - 18732  5 - 2718  W - 2718  T - 187	Flume Data  40 - 1929  6 - 1939  8 - 1938  9 - 2-18  9 - 2-19  7 - 121  1 - 3-2	Flume Data  *** - 18729  8 - 18729  8 - 18729  \$ - 25118  9 - 352  T - 182  H - 252	Flume Data  4A = 18929  4C = 1999  8 = 1119 M  5. = 24118  W = 344  T = 144  H = 948	Flume Data  44 - 18128  47 - 11028  8 - 11128  51 - 24118  W - 341  T - 121  H 3542
Curve Data (A) (B) (C) (C) (C) (C) (C) (C) (C) (C) (C) (C	Curve Data  C  13	Curve Data  C1.  18 = 31-464  19 = 19-464  10 = 19-464  10 = 19-464  10 = 19-464  10 = 19-464  10 = 19-464  10 = 19-464  11 = 19-464  11 = 19-464  11 = 19-464  11 = 19-464  11 = 19-464  11 = 19-464  11 = 19-464	Curve Data  Gue  1 - 1  0 - 15446  0 - 15446  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 15466  0 - 154666  0 - 154666  0 - 154666  0 - 154666  0 - 154666  0 - 154666  0 -	Curve Data  CL  CL  CL  CL  CL  CL  CL  CL  CL  C	Curve Data (5.2) (5.3) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4) (5.4)	Curve Data ct 214-48 0 - 214-48 0 - 104-68 0 - 104-68 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-78 0 - 105-7





7'x5' Flume Chute - Longitudinal Section



relaht of ba	rs over 40 0 Tong Include an	
Howance for	r a 2:0 lap but lengths shown	
	40 0 long do not include	

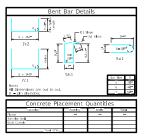
		Chute Length (C.L.)	-
2 Section 2	<del></del>	? Section 1	
ļ	Length	13 0	ength
		5u1 fence anchor to be placed at direction of Engineer	
Measure of Tonic (Top Well Trans)	401 6		\$11.5 x23
60		Flared Bars: Maintain the horizontal spa- for 4a1.6 5c1 bars along II	cing gwiling.
Townson X 3	ed bars 4a1 & 5c1; minimum 1.5 bar spacing maximum do not exceed 18 inches	Note: Bars Sc1 & 6m1 are elmin at flume chute joint.	
		Bars Soa @ 1 0 , c1, c2 6 5c3 Bars Sp	

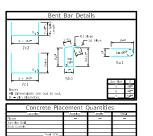
+ 1·2* 7c2	ii -	5u1 s: 5tm D 5 3g 6 4g 7 5g	<del>* </del>
ement C	)uantities	;	
Footing	Wals	Total	Notes:  1. See Sheeks plainmatten 2. See Sheeks 3. See Sheek R 18 beeks 19 See Sheek R

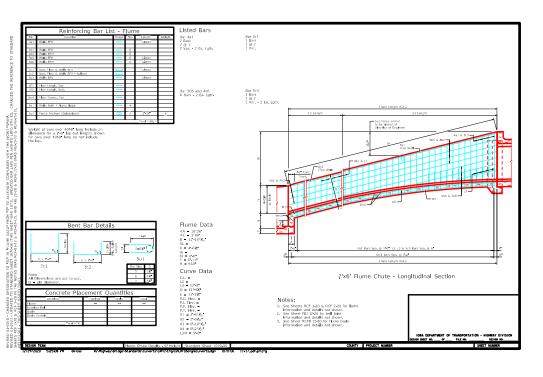
bent	Dai Deta	1115	
s + 1 · 2 s ?c1  Note: Al Dimensions are out to out. D - pla diameter.	0 () (+ ) 2* 7c2	In Spirit	5u1  5x 5v 0  5 3x 6  6 4x 7  5 5x
Concrete Plac	cement (	)uantitie	S
Location	Footing	Wals	Total
Flame - Section 1	_		_
Flame - Section 2			
Junction Bell Chute Bell			
Chate Bell Bestn			

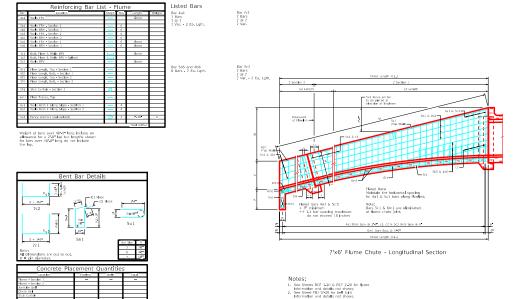
### 7'x5' Flume Chute - Longitudinal Section

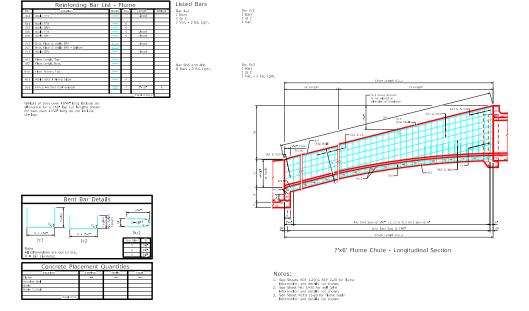
4:1 SLOPE FLUME							
x 5	6 x 5	8 x 5	10 x 5	12 x 5	14 x 5	16 x 5	
Flume Data  (4 - 34°02  46 - 31°02  47 - 31°02  48 - 35°31 V <sub>6</sub> 48 - 30°3  48 - 30°3  48 - 30°3  48 - 30°3  48 - 30°3  48 - 30°3	Flume Data  6A = 14/30  6A = 14/30  6E = 16/31 / A  5E = 3 × 16/4  6F = 3 × 16/4  F = 6/4 / A  F = 6/4 / A	Flume Data  44. – 14/027  46. – 15/17/4,  5. – 7. – 5/18/4,  W – 9/27  T – 1/07  H = 5/07	Flume Data  A = 14-000  B = 14-000  S = 10-000  V = 2-000  V = 2-00  V = 2-00  H = 3-00	Flume Data  40 - 14000  60 - 15000  70 - 25000  71 - 150  71 - 150  71 - 150  71 - 150  71 - 150  71 - 150	Flume Data  4A = 34'02' 4C = 3'00' 8 = 35'3'''A; 5	Flume Data  44 - 14002  45 - 17007  8 - 1813 976  51 - 311007  W - 311007  H - 3217  H - 3247	
Curve Data 5.5. 3 - 29096. 5 - 10.1096 10.1096 10.1096 10.1096 10.1096 10.1096 10.1096 10.1096 10.1096 10.1096 10.1096.	Curve Data  C	Curve Data  CA -	Curve Data  (1) (2) (3) (4) (4) (5) (5) (6) (6) (7) (6) (7) (7) (7) (7) (7) (7) (7) (7) (7) (7	Curve Data  GL -  GL -	Curve Data  2.	Curve Data  c  3 - 20-98.  0 - 181-98.  c - 181-98.  c - 181-98.  c - 181-98.  c - 181-98.  d - 188.  d	



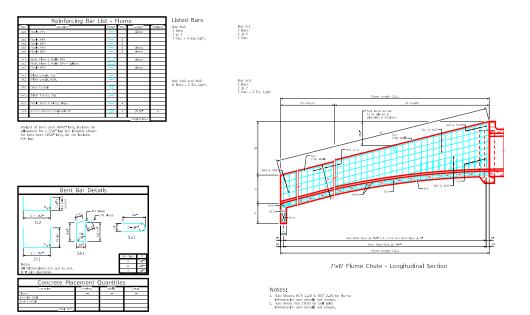


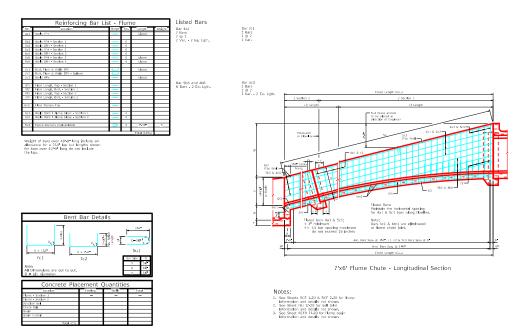


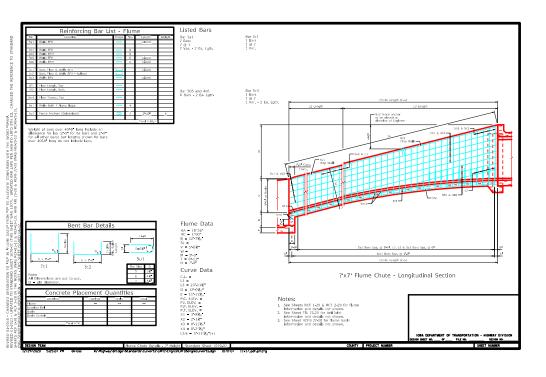


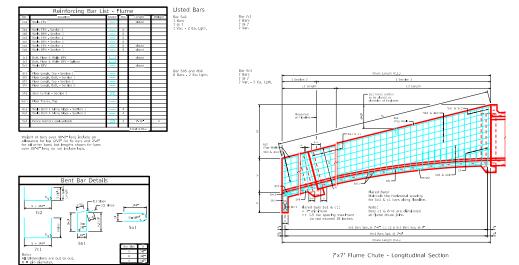


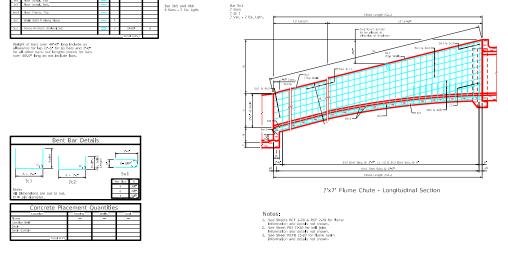










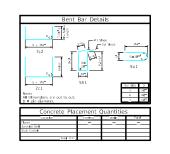


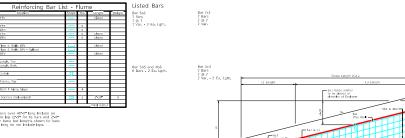
6 x 7	8 x 7	$10 \times 7$	12 x 7	14 x 7	16 x 7
Flume Data  4A = 18*20* 4C = 17*00* 8 = 12*2*786* 9 = 5 * 5 * 6 * 8  W = 5 * 5 * 3* T = 0*.11* H = 7**-0*	Flume Data  4A = 18725  4C = 1190  B = 12.776  SL = v = 5.630  M = 5.3  T = 1.0  H = 7.0	Flume Data  4.4 = 18739  4.5 = 12.79(-5)  5. = 7.5 - 58,  W = 5.5 - 58,  H = 7.5 - 79,  H = 7.5 - 79,	Flume Data  4A - 18*20* 4C - 1*00* B - 12*-7%; SL = V - 5*-6%; W = 5*-3* T - 1*-2* H = 7*-0*	Flume Data  4A 18726  4C 11700  8 - 12774;  SL =  V - 57-64; W = 57-3  T - 1727  H = 77-0	Flume Data  4A - 18*20* 4C = 1100* 8 - 12*7/K/r* St = V - 5*6*K* W = M - 5*3* T - 1*2* H = 7*0*
Curve Data	Curve Data	Curve Data	Curve Data	Curve Data	Curve Data
CAL = 1.17	C	C.L. = 12 - 12 - 12 - 12 - 12 - 12 - 12 - 12	C1. = 13 = 23×11½ 0 = 12×11½ 0 = 12×11½ 0 = 11×11½ 0 = 11×11½ 0 = 11×11½ 0 = 11×11½ 0 = 11×11½ 0 = 11×11½ 0 = 0 = 11½ 0 = 0 = 11½ 0 = 0 = 0 = 11½ 0 = 0 = 0 = 11½ 0 = 0 = 0 = 11½ 0 = 0 = 0 = 11½ 0 = 0 = 0 = 11½ 0 = 0 = 0 = 11½ 0 = 0 = 0 = 11½ 0 = 0 = 0 = 11½ 0 = 0 = 0 = 0 = 11½ 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 =	CL = 23-11½" D = 12-20½" E = 112-11½, P.C. ELEV. – P.J. ELEV. – P.J. ELEV. – P.J. ELEV. – 23 – 23-1½, 24 – 02-2½, 24 – 02-2½, 24 – 02-2½,	CL = 12 13 = 23-11 K O = 12-0 K, E = 11-11 K, P.C. ELEV. – P.F. ELEV. – P.T. ELEV. – P.T. ELEV. – 23 = 2-1 K, 24 = 0-2 K, 24 = 0-2 K, 24 = 0-2 K, 25 = 2-1 K,

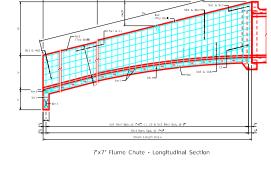
### 4.1 SLOPE FLUME

6 x 7	8 x 7	10 × 7	12 x 7	14 × 7	16 x 7
Flume Data  4A = 14*02* 4C = 1700* 8 = 17*38* 5. = 5. V = 5.5 V = 0.11* H = 7*0-11* H = 7*0-1	Flume Data  4A = 14*02* 4C = 1*00* 8 = 17*3k* 9 = 5*5* W = 5*5* T = 1*0* H = 7*0*	Flume Data  4A - 1400* 4C - 1700* 8I - 177-59* V - 57-5* W - 37-9 H - 17-7* H - 7-7*	Flume Data  4A = 14*02* 4C = 1*00* B = 1*7*38* S = 5*3* W = 5*3* T = 1*2* H = 7*3*	Flume Data  4A - 14*02* 4C = 17*00* 8 - 17*34* \$1 = 17*34* \$1 = 5*-5* W = 5*-3* T = 1*-2* H = 7*-0*	Flume Data  4A = 14*02* 4C = 1*00* B = 1*7*-38** SL = 5*-5** M = 5*-3* T = 1*-2* H = 7*-0*
Curve Data	Curve Data	Curve Data	Curve Data	Curve Data	Curve Data
CAL 2 = 13 - 17 kg. 0 = 10 - 10 10 kg. E - 16 10 7 kg. P.C. CLEV. = 10 1 10 kg. P.C. CLEV. = 10 10 kg.	C.L. (2 = 13 - 33 - 7 M <sub>A</sub> ) D = 16 - 16 M <sub>A</sub> E = 16 - 9 M <sub>A</sub> P.C. ELEV. = P.E. ELEV. = P.E. ELEV. = (3 - 3 - 16 M <sub>A</sub> ) X = 2 - 2 M <sub>A</sub> X = 0 - 11 M <sub>A</sub> X = 0 - 11 M <sub>A</sub> X = 0 - 2 M <sub>A</sub> X = 0 - 2 M <sub>A</sub> X = 0 - 2 M <sub>A</sub>	C1. — 1.2 = 1.3 - 23.7   Z <sub>1</sub> = 1.3 - 23.7   Z <sub>2</sub> = 1.3 - 23.7   Z <sub>1</sub> = 1.0   100   Z <sub>2</sub> = 1.0   100   Z <sub>2</sub> = 1.0   Z <sub>2</sub> =	C.L.  (2 = 13 - 33.7/V <sub>A</sub> )  D = 16-10/W  E = 16-9/W  P, CLEV. = PL ELEV. = P.	C.L. = 1.2 = 1.3 = 337.71% D = 10°-10% E = 10°-90% P.C. ELEV. = P.J. ELEV. =	C.1.  L2 = 33.73°M <sub>c</sub> D = 16.10°M' E = 16.90°M' P.C. ELEV. = P.I. ELEV. = P.P. ELEV





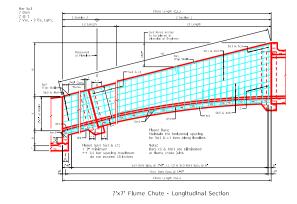




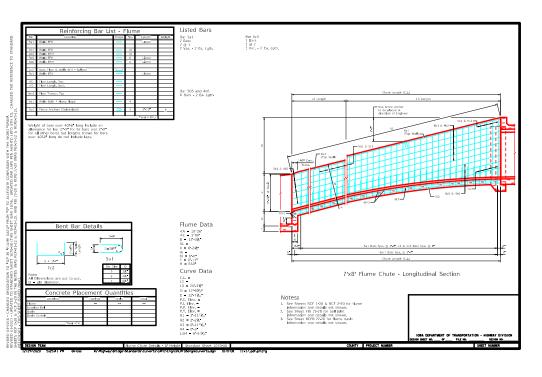
	otes:
1.4	Jica.
1.	See Sheets RCF 1 20 & RCF 2 20 for flume
	Information and details not shown.
2	See Sheet FBJ ??-20 for bell joint









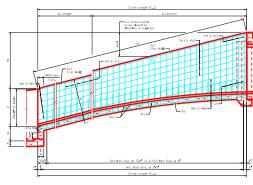






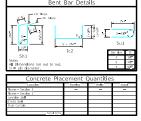






?'x8' Flume Chute - Longitudinal Section

Notes:
1. See Sheets RCF 1-2
Information and de
2. See Sheet FBI ??-2
Information and de
2 Con Chart DCCD 22



?'x8' Flume Chute - Longitudinal Section

Moesured at Flouine —

Flared Bars: Maintain the horizontal spacing for Sa1, c2 & Ec5 bars along flowline. Noce: Bars c2, 5c3 6 6m1 are of minated at flume chute joint.

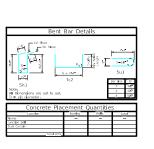
3:1 SLOPE FLUME

6 x 8	8 x 8	10 x 8	12 x 8	14 x 8	16 x 8
Flume Data  4A = 18°26' 4C = 1°100' 8 = 18'-38'' 9L = 0'-38', W = 6'-0' T = 0'-11' H = 8'-0'	Flume Data  46 - 18756* 46 - 18756* 47 - 18758* 58 - 18758* 79 - 6738* 89 - 6745* 11 - 875*	Flume Data	Flume Data <a 18*28*="" 6*38*="" <c="19*00*" =="" b="13*380*" h="18*0*&lt;/td" s="V" t="1/2*" w="6*30*"><td>Flume Data  44 - 18*28*  45 = 1*00*  8 - 13*38*  V = 6*38*  W = 6*0*  T = 1*2*  H = 8*0*</td><td>Flume Data  4A = 18726  4C = 1700  B = 181-384  SL = 3-38  W = 6-38  M = 6-27  T = 17-2  H = 8-0</td></a>	Flume Data  44 - 18*28*  45 = 1*00*  8 - 13*38*  V = 6*38*  W = 6*0*  T = 1*2*  H = 8*0*	Flume Data  4A = 18726  4C = 1700  B = 181-384  SL = 3-38  W = 6-38  M = 6-27  T = 17-2  H = 8-0
Curve Data C.I. =  1.1 = 22-38 0 = 12-86 0 = 12-86 0 = 12-86 0 = 12-86 0 = 12-86 0 = 12-86 0 = 12-86 0 = 12-86 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180 0 = 180	Curve Data  cs	Curve Data CD - 1 CD -	Curve Data CL = 13 = 23-347 D = 124-347 D = 124-347 E = 124-347 PC flex = 104 slex = 105 slex = 107 slex = 107 slex = 108 slex = 109	Curve Data CL = 1.3 = 22-3/K D = 22-3/K D = 12-3/K E = 12-7/K PC Gev = PC Gev = PC Gev = PC Fixe	Curve Data CL = 13 = 23-18/ 0 = 12-88/ 0 = 12-88/ 0 = 12-78/ 0 C Elex - 13 Hex = 15 Hex = 17 Hex = 17 Hex = 18
	4:1	SLOPE	FLUME		

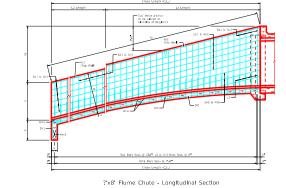
	111 32312 123112							
5 x 8	8 x 8	10 x 8	12 x 8	14 x 8	16 x 8			
Flume Data <a 14*02*="" 6*28*="" <c="1*00*" =="" b="18*38*" h="8*0*&lt;/td" st="V" t="0*-11*" w="8*0*"><td>Flume Data  40 = 14*00*  40 = 1*00*  8 = 18*390*  S. =  V = 6*24*  M = 6*40*  H = 8*40*</td><td>Flume Data  \$A = \$40000 \$C = \$1000 B = \$1000 S = \$0 = \$0.00 W = \$6.00 M = \$6.00 H = \$6.00</td><td>Flume Data  4.4 - 14*02* 4.5 - 2*00* 8 - 18*38* 5.1 - 18*38* V - 6*28* W - 6*39* H = 8*37*</td><td>Flume Data  <a 14*02*="" 6*28*="" <c="1*00*" =="" b="18*38*" h="8*0*&lt;/td" sl="V" t="1*2*" w="1*2*"><td>Flume Data  4A = 14*02* 4C = 1*00* B = 18*3%* SL = V = 6*2K* W = M = 6*40* T = 1*2* H = 8*-0*</td></a></td></a>	Flume Data  40 = 14*00*  40 = 1*00*  8 = 18*390*  S. =  V = 6*24*  M = 6*40*  H = 8*40*	Flume Data  \$A = \$40000 \$C = \$1000 B = \$1000 S = \$0 = \$0.00 W = \$6.00 M = \$6.00 H = \$6.00	Flume Data  4.4 - 14*02* 4.5 - 2*00* 8 - 18*38* 5.1 - 18*38* V - 6*28* W - 6*39* H = 8*37*	Flume Data <a 14*02*="" 6*28*="" <c="1*00*" =="" b="18*38*" h="8*0*&lt;/td" sl="V" t="1*2*" w="1*2*"><td>Flume Data  4A = 14*02* 4C = 1*00* B = 18*3%* SL = V = 6*2K* W = M = 6*40* T = 1*2* H = 8*-0*</td></a>	Flume Data  4A = 14*02* 4C = 1*00* B = 18*3%* SL = V = 6*2K* W = M = 6*40* T = 1*2* H = 8*-0*			
Curve Data  CL  (L) =  12 = 35.7%;  D = 17.10%;  E = 17.0%;  PC. Glev. =  PP. Glev  PP. Glev  PP. T. Hev. =  XI - 44.7%;  XI = 25.2%;	Curve Data c.t. 12 = 13 - 35-7% 0 = 17-10% 15 - 17-90 15 - 18-0 16 - 18-0 17-90 18-0 18-0 18-0 18-0 18-0 18-0 18-0 18-	Curve Data  CL 12 = 13 - 35 - 7 Nr.  D = 17 - 10 Nr.  PC. Elec. = 17 - 9 Nr	Curve Data  CA  12 = 13 - 35 - 7 V <sub>a</sub> 0 = 13 - 10 V <sub>b</sub> E - 37 - 9 V <sub>b</sub> PC. Bev. = P. Bev.	Curve Data ct 12 = 13 - 35-7%, D = 17-10%, E - 17-10%, P.C. Elev. = P.C. Blev. = P.C. Blev. = P.C. Blev. = 21 - 4-1%, 22 = 2-32"	Curve Data  C.L 12 = 13 - 35 - 7 Mr  D = 17 - 10 Mr  E - 17 - 9 Mr  P.C. Elev. = P.F. Elev P.F. Elev. = X1 - 4 - 1 Mr  X2 = 2 - 3 Mr			
A2 = 2 -96 X3 = 1 -08 X4 = 0 -386 L3/4 = 8 -10 R <sub>0</sub> (+)	X3 = 0.3N°. X3 = 1.0N. X3 = 5.3N°.	X3 = 1 · 0 X X4 = 0 · 3 X <sub>0</sub> X3 = 1 · 0 X X = 2 · 3 X	X2 = 2-3K" X3 = 1-0K" X4 = 8-10 <sup>4</sup> K <sub>2</sub> (+)	$XZ = Z - 3X_{c}$ $X3 = 1 - 0X_{c}$ $X4 = 0 - 3X_{c}$ $L3/4 = 8 - 10^{1}X_{c}$ (+)	X2 = 2 3 % X3 = 1 0 % X4 = 0 3 %; L3/4 = 8 10 1 %; (+:			

Section   Sect	331	Location	Shape	160	Length	Whight
See Section	551	Walls FFV	_		Usted	
See Section	561	Walls FFH		10		-
200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200   200	102	Wels SPH		10		-
bec. ther & with the values	030		_			
Well at Y	156	Walls BPH	_	С	United	
Ther tong, Tag	No 2	Bott, Floor & Walls BEV - Soliced	_	_		-
1 Sub-Curtin II	313	with pry	_		Lived	
1 Sub-Curtin II	611	Fluor Long Ton		_		-
Hace Transy, Top	502		_			
	5h1	Stub Curtain				$\vdash$
1 Wells Both F Along Slope - 4	im1	Place Transv. Top	_			
	61	Wells Both F Along Slope	_	4		
1 Fence Archors (Galvanted) 2 2-10* 6	Sul	Fence Archors (Galzanfred)	_	2	2 10	- 6_

Weight of bars over 40.0° long include an allowance for lap (2.5° for 6s bars and 2.0° for all other bars) but lengths shown for bars over 40.0° long do not include laps.



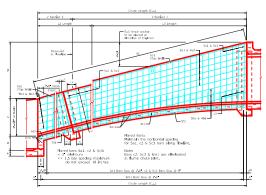




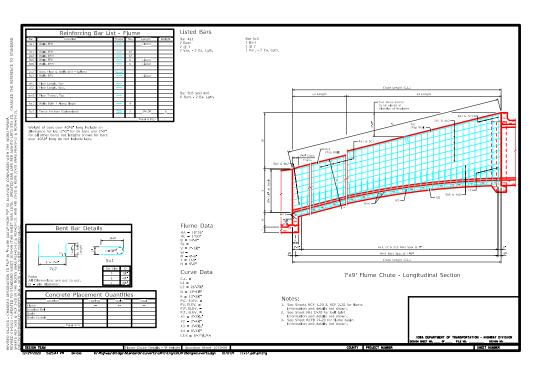
	Reinforcing Bar	List - I	lun	ne .		Listed Bars
ar al	Location	Shape	No.	Length	Weight	Bar 5a1
Ä	Walls FFV	_		Usted		? Bars
						7 @ 7
	Wells FFH - Section 1	_	10			? Var. • 2 Ea. Lgth.
2	Wells BTH - Section 1	_	10			
2	Wells FFH - Section 2	_	10			
T.	Walls BFH - Section 2	_	10			
ō,	With FFH - Section 1		- 6	Usted		
δ	Wills BFH - Section I	_	- 6	Usted		
_		_	_			
2	Boll, Floor & Walls BPV - Spiced	_	_		-	
3	Wats 8FV		_	Urited		
1	Floor Longit, Top - Section 1	_	_			
	Floor Long F. Top - Section 1		_			Bar 5b5 and 4b6
3	Floor Long C. Section 1 Floor Long C. Top - Section 2		_		-	6 Bars - 2 Ea. Lgth.
3	Floor Longt, Bott, Section 2		_		_	
-	FOOT LONGS, 800, 4 SECTOR 2		_		_	
	Floor Transy-Top		_		_	
	The control of		_		_	
	Walls Roth F Along Stope - Section 1		4			
2	Walls Both F Along Stope - Section 2		4			
-	, , , , , , , , , , , , , , , , , , , ,		-			
	Fence Anchors (Galvanted)		2	2.10	- 6	

Bent Bar Details				
S+3-4  Scale State		5 3X 5 5 3X 6 4X 7 5X		
Concrete Plac	cement (	Duantitie	s	
tocation	Footing	Walk	Total	
Hume - Section 1				
Hume - Section 2				
Junction Bell Chute Bell				
Rada				
	_	_		
Basin Curtain				

Bar Sc3 ? Bers ? @ ? ? Var. - 2 Ea. Lgth.

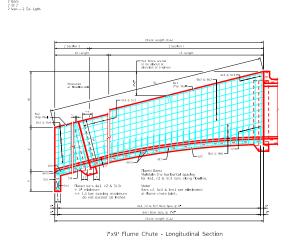


?'x8' Flume Chute - Longitudinal Section

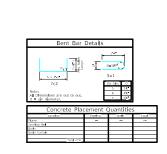


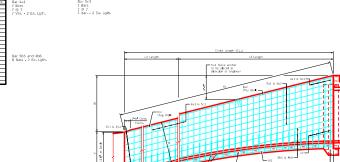






Sulfence anchor to be placed at direction of Engineer





7'x9' Flume Chute - Longitudinal Section

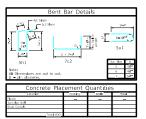
# 3:1 SLOPE FLUME

8 x 9	10 × 9	12 x 9	14 x 9	16 x 9
Flume Data  4A - 18*20  4C = 1*900  8 - 14*-0  SL = V - 7*-1%  W - 7*-1%  W = 6*-9  T - 1*-0  H = 9*-0	Flume Data <a -="" 1*-1*="" 14*0*="" 18*26*="" 7*118*="" <c="19*00*" b="" h="9*-0**&lt;/td" m="6*-9**" st.="V" t="" w=""><td>Flume Data  4A = 18°26' 4C = 1'00' 8 = 16'-0' SL = V = 7'-1'8'' W = 6'-9' T = 1'-2' H = 9'-0'</td><td>Flume Data  4A = 18126  4C = 1100  B = 144.0  SL = V = 71.38  W = 6-9  T = 112  H = 9.90</td><td>Flume Data  4A = 18128  4C = 1100  B = 1440  SL = V = 7118  W = 6-9  T = 112  H = 9-0</td></a>	Flume Data  4A = 18°26' 4C = 1'00' 8 = 16'-0' SL = V = 7'-1'8'' W = 6'-9' T = 1'-2' H = 9'-0'	Flume Data  4A = 18126  4C = 1100  B = 144.0  SL = V = 71.38  W = 6-9  T = 112  H = 9.90	Flume Data  4A = 18128  4C = 1100  B = 1440  SL = V = 7118  W = 6-9  T = 112  H = 9-0
Curve Data	Curve Data	Curve Data	Curve Data	Curve Data
C.L. = 1.0 - 176.   D - 13'-4K'   E - 11'-3K'   E - 11'-3K'   P.C. ELEV   P.E. ELEV   P.E. ELEV   AT - 4'-2K'   X2 - 2'-4K'   X3 - 1'-0K'   X4 - 0'-3K'   X4 - 0'-3K'   X4 - 0'-3K'   X4 - 0'-3K'   X5 - 1'-0K'   X6 - 0'-3K'   X7 - 1'-0K'   X8 - 1'-0K'   X9 - 1'-0K'    X9 - 1'-0K'   X9 - 1'-0K'    X9 - 1'-0K'    X9 - 1'-0K'    X9 - 1'-0K'	C.L. = 12 - 20 - 76	C.L. = 12 - 28 - 78 - 13 - 28 - 78 - 13 - 28 - 78 - 13 - 28 - 78 - 13 - 28 - 28 - 28 - 28 - 28 - 28 - 28 - 2	C.L = 13 - 26 - 7/K   D = 13 - 46 / 7   E = 13 - 38 / 7   E = 13 - 38 / 7   E = 14 - 38 / 7   E = 14 - 28 / 7   E = 14	CL = 13 - 28 - 7% D = 13 - 48 E = 13 - 48 E = 13 - 38 PP, EHV. = PP, EHV. = PT, EHV. = EHV. = PT, EHV. = EH

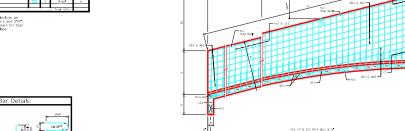
# 4:1 SLOPE FLUME

8 x 9	10 × 9	12 x 9	14 x 9	16 × 9
Flume Data  4A = 14*02* 4C = 14*02* 4C = 17*00* 8 = 18*-33*96* SL = V = 0.11 K W = 0.9 T = 11.0* H = 9.9 T = 12.0*	Flume Data <a -="" 1*-1*="" 14*02*="" 19*31*="" 6*.9*="" 6*11*="" 8="" <c="1*00*" c="" c,="" h="9*-0*&lt;/td" st.="V" t="" w=""><td>Flume Data  4A - 14*02* 4C = 1*00* 8 - 19*3*½, SL = V - 6*11½, W - M = 6*9* T - 1*2* H = 9*0*</td><td>Flume Data  <a -="" 0="" 1'-2'="" 14'02'="" 19'3'½'="" 6'-11½'="" <c="1'00'" h="9'-0'&lt;/td" s.="V" t="" w=""><td>Flume Data  «A - 14*02* «C = 1*00* B - 18* 3*1%; St = V - 6* 11%; W - 6* 11%; H = 6* 9* T - 1*.2* H = 9* 0*</td></a></td></a>	Flume Data  4A - 14*02* 4C = 1*00* 8 - 19*3*½, SL = V - 6*11½, W - M = 6*9* T - 1*2* H = 9*0*	Flume Data <a -="" 0="" 1'-2'="" 14'02'="" 19'3'½'="" 6'-11½'="" <c="1'00'" h="9'-0'&lt;/td" s.="V" t="" w=""><td>Flume Data  «A - 14*02* «C = 1*00* B - 18* 3*1%; St = V - 6* 11%; W - 6* 11%; H = 6* 9* T - 1*.2* H = 9* 0*</td></a>	Flume Data  «A - 14*02* «C = 1*00* B - 18* 3*1%; St = V - 6* 11%; W - 6* 11%; H = 6* 9* T - 1*.2* H = 9* 0*
Curve Data	Curve Data	Curve Data	Curve Data	Curve Data
C.L. = 12 - 37-61/6 D - 18-97/6 E - 18-98/7 E - 18-98/7 E - 18-98/7 P.C. EEEV. = P.F. EEEV. = P.T. EEEV. = X1 - 47-45/6 X2 = 2'-5/8 X3 - 2'-18/6 X4 = 0'-3/8 X5 = 0'-3/8 X6 = 0'-3/8 X7 = 0'-3/8 X7 = 0'-3/8 X7 = 0'-3/8 X8 =	C.L. = 13 - 37 - 6782. D - 18 - 37 - 6782. D - 18 - 98 - 98 - 6 - 18 - 18 - 18 - 18 - 18 - 18 - 18	C.L. = 1.2 - 3.7 - 6 / M <sub>2</sub> D - 16 / 6 / M <sub>2</sub> E - 16 / M <sub>2</sub> E - 16 / M <sub>2</sub> E - 2 / M <sub>2</sub>	C.L = C.L = 12 - 37-61/H,   0 - 10'-9'/K,   0	C.L. = 1.2 - 18.49 %; D - 18.49 %; E - 18.48 %; P.C. ELEV. = P.J. ELEV. = ELEV.

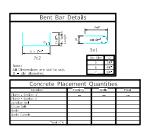


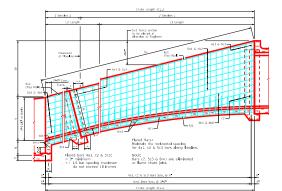


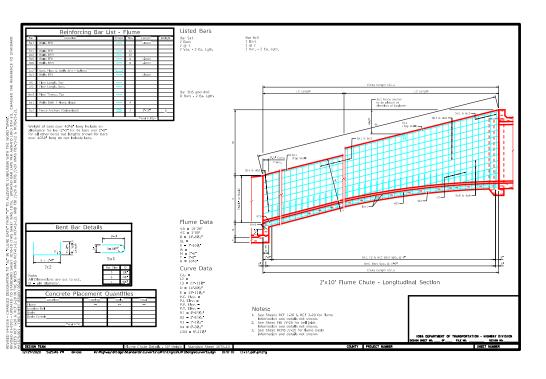


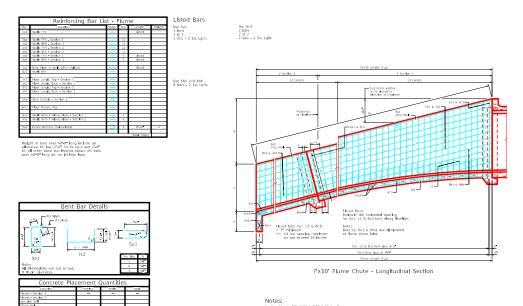


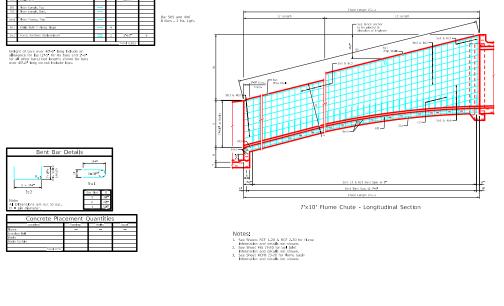
	ReInforcing Bar	List - I	lun			Listed Bars
161	Location	Shape	No.	Length	Wealth	Bar 4a1
7	Walls FFV	ı		Usted		2 Bars 7 @ 7
						? Var 2 Ea. Loth
b1	Wals FFH - Section 1	_	_12_			: vai 2 ca. byti
24	Wals Still - Section 1	_	12		_	
153	Walls FFH - Section 2	_	12			
ž.	Walls BFH - Section 2	_	12		_	
16	Wats FFH - Section 1 Wats BFH - Section 1	_	- 6	Usted	_	
166	Wals BH - Section 1	_	- 6	Usted	_	
45	Bott, Floor & Watts BFV - Spired		_			
(3	Was RPV			Histori	_	
11.5	Mate on			Usico	_	
543	Floor Longit, Top - Section 1		_			
512	Floor Longt, Bott - Section 1					Bar 5b5 and 4b6
9/3	Floor Long*, Top - Section 2		_			6 Bars • 2 Ea. Lgt
554	Floor Longit, Bott, - Section 2					
mì	Hoor Transy, Too	_				
						l
561	Walls Both F Along Slope - Section 1	_	-4			
42	Walls Both F Along Slope - Section 2	_	-4			
						l
103	Fence Anchors (Galvantred)		2	2 10	6	l
				Total (LBS.)		











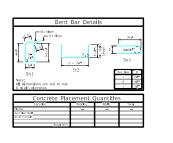
	Flume Data
Flume Data Flume Data Flume Data Flume Data	
4A - 18'26' 4A - 18'26' 4A - 18'26' 4A - 18'26'	∢A = 18*26*
«C = 1°00° «C = 1°00° «C = 1°00°	«C = 1'00'
$B = 14.8\%_0$ $B = 14.8\%_0$ $B = 14.8\%_0$ $B = 14.8\%_0$	B = 14 8% <sub>6</sub>
SL= SL= SL= SL= V=7-10% V=7-10% V=7-10%	SL = V = 7-10Z
W= 1-10% V= 7-10% V= 7-10%	W = 7-10%
M = 7.6 M = 7	M = 7.6
$\dot{T} = P \dot{\Omega}^{\dagger}$ $\dot{T} = P \dot{\Omega}^{\dagger}$ $\dot{T} = P \dot{\Omega}^{\dagger}$ $\dot{T} = \dot{P} \dot{\Omega}^{\dagger}$	T = 1.2
H = 10-0 H = 10-0 H = 10-0	H = 10.0
Curve Data Curve Data Curve Data Curve Data	Curve Data
CL - CL - CL -	C.L
12 12 12	L2 =
L3 = 27-11K L3 = 27-11K L3 = 27-11K L3 = 27-11K	L3 = 27.11½
D = 14.0N <sub>0</sub> D = 13.11N <sub>0</sub> D = 13.11	D = 14.0% E = 13.11%
P.C. Elev P.C. Elev P.C. Elev P.C. Elev	P.C. Elev. =
P.L. Elev.	P.L. Elev.
P.P. Elev P.P. Elev P.P. Elev P.P. Elev	P.P. Elev
P.T. Elev.	P.T. Elev
X1 = 0.41%, $X1 = 0.41%$ , $X1 = 0.41%$ , $X1 = 0.41%$ ,	×1 = 4-4 <sup>1</sup> N <sub>0</sub> *
x2 = 2 s N <sub>2</sub>	X2 = 2 -5 <sup>1</sup> N <sub>6</sub>
$x_3 = 1.1 N_0$ , $x_3 = 1.1 N_0$ , $x_3 = 1.1 N_0$ , $x_3 = 1.1 N_0$	$X3 = 1 - 1 N_0$
$X4 = 0^{\circ} 3N_0$ $X4 = 0^{\circ} 3N_0$ $X4 = 0^{\circ} 3N_0$ $X4 = 0^{\circ} 3N_0$	X4 = 0-3 N <sub>0</sub>
L3/4 = 6-11%" L3/4 = 6-11%" L3/4 = 6-11%" L3/4 = 6-11%"	L3/4 = 6.11%

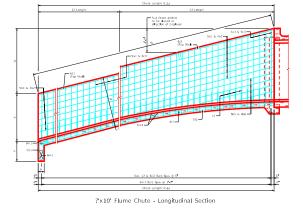
# 4:1 SLOPE FLUME

8 x 10	10 × 10	12 × 10	14 × 10	16 × 10
Flume Data  4A = 14/02' 4C = 17/00' 8C = 27/33/4/6' SL = 27/33/4/6' W = 7/6' T = 17/4' H = 17/6' H = 17/6'	Flume Data <a -="" 1*-1*="" 14*02*="" 20="" 3*f4*="" 7*8*k*="" <c="1*00*" b="" h="10*-0*&lt;/td" sl="V" t="" w="7*6"><td>Flume Data  <a 14'02'="" 7'8\(\mathred{h}_{i}\)="" 8="20'3'\(\mathred{H}_{i}\)" <c="1'00'" =="" h="10'0'&lt;/td" sl="V" w="1'8\(\mathred{H}_{i}\)"><td>Flume Data  4A = 14'02' 4C = 1'00' 8 = 20'3'\%, \$L = V = 7'3\%, W = 7'3\%, H = 10'0' H = 10'0'</td><td>Flume Data  4A - 14*02* 4C = 1*00* B - 20*3*Fa* SL = V - 7*8* W = 7*6* T - 1*2* H = 10*0*</td></a></td></a>	Flume Data <a 14'02'="" 7'8\(\mathred{h}_{i}\)="" 8="20'3'\(\mathred{H}_{i}\)" <c="1'00'" =="" h="10'0'&lt;/td" sl="V" w="1'8\(\mathred{H}_{i}\)"><td>Flume Data  4A = 14'02' 4C = 1'00' 8 = 20'3'\%, \$L = V = 7'3\%, W = 7'3\%, H = 10'0' H = 10'0'</td><td>Flume Data  4A - 14*02* 4C = 1*00* B - 20*3*Fa* SL = V - 7*8* W = 7*6* T - 1*2* H = 10*0*</td></a>	Flume Data  4A = 14'02' 4C = 1'00' 8 = 20'3'\%, \$L = V = 7'3\%, W = 7'3\%, H = 10'0' H = 10'0'	Flume Data  4A - 14*02* 4C = 1*00* B - 20*3*Fa* SL = V - 7*8* W = 7*6* T - 1*2* H = 10*0*
Curve Data	Curve Data	Curve Data	Curve Data	Curve Data
C.L. = 1.2 - 1.3 - 39'-4K',   D - 19'-4K'   E - 19'-4K'   E - 19'-4K'   P.C. Glev = P.L. Hev. = P.L. Hev. = P.T. H	CL = (2 - 39°-6 M <sub>2</sub> ) 13 - 39°-6 M <sub>2</sub> ) 10 - 19°-6 M <sub>2</sub> ; 11 - 19°-6 M <sub>2</sub> ; 12 - 19°-6 M <sub>2</sub> ; 13 - 19°-6 M <sub>2</sub> ; 134 - 9°-6 M <sub>2</sub> ; 135 - 9°-6 M <sub>2</sub> ; 135 - 9°-6 M <sub>2</sub> ; 135 - 9°-6 M <sub>2</sub> ; 136 - 9°-6 M <sub>2</sub> ; 137 - 9°-6 M <sub>2</sub> ; 137 - 9°-6 M <sub>2</sub> ; 137 - 9°-6 M <sub>2</sub> ; 138 - 9°-6 M <sub>2</sub> ; 139 - 9	C,1, = (2, 2) = (3, 4) = (3, 4) = (3, 4) = (3, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4) = (4, 4	C.L. = C. = 29-474, D = 19-947, E = 19-187, P.C. Hew = P.F. Hew = P.T. Hew = P.T. Hew = X.L. 47-75, X.E. = 2-675, X.E. = 0-136, X.E. = 0-136, X.E. = 0-136,	CL = 12 - 39 - 5 / K, D - 19 - 5 / K, E - 19 - 6 / K, P.C. Hev. = P.I. Hev. = V.I 4 / K, X = 2 - 6 / K, X = 1 - 1 / K, X = 0 - 1 / K, 124 - 9 - 1 / K, 125 - 9 - 1 / K, 126 - 9 - 1 / K, 127 - 9 - 1 / K, 128 - 9 - 1 / K, 129 -





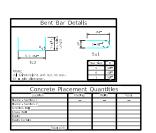


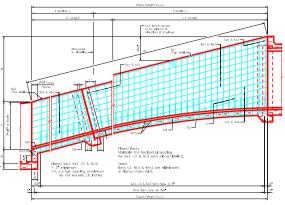


Notes:
1. See Sheets RCF 1-20 & RCF 2-20 for flume Information and details not shown.
2. See Sheet FBI 27-20 for bell joint Information and details not shown.



Ight of bars over 40°-0" long Include an wance for Igo (2-3" for 6s bars and 2-0all other bars) but lengths shown for bars or 40°-0" long do not include laps.

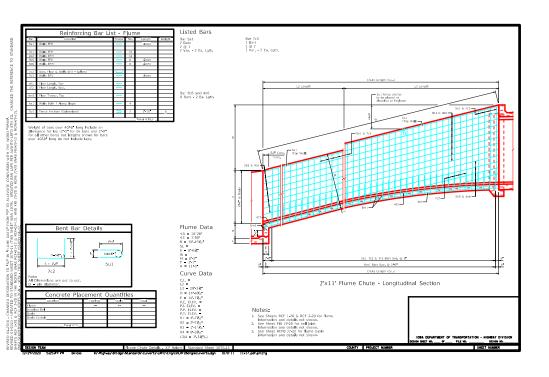




?'x10' Flume Chute - Longitudinal Section

otes: See Sheets RCF 1-20 & RCF 2-Information and details not sho

See sneets for 1-20 a for 2-20 in filling Information and details not shown. See Sheet FBJ 72-20 for bell joint Information and details not shown. See Sheet RCFB 72-20 for filling basin before a fill of the shown.



Flume Data

4.6 = 18200

8. = 1544 Mg.

8. = 1544 Mg.

9. = 1648 Mg.

9. = 1648 Mg.

11. = 11.01

Curve Data

Cu. =

10. = 14.04 Mg.

10. = 14

12 x 11 14 x 11 16 x 11

Flume Data

4A = 1979

4A = 1979

5 = 13444/4

5 = 13444/4

5 = 13444/4

6 = 13444/4

1 = 1144

Curve Data

Cu. = 100

1 = 1444/4

E CEUX - 100

2 = 1444/4

E CEUX - 100

E CEUX

Flume Data

40 = 1920

40 = 1920

50 = 1344/6

51 = 348/6

70 = 818/7

71 = 1149

Curve Data

Cur, Curve Data

Cu, Curve Data

Curve D

10 x 11

Flume Data

\*A = 18736

\*C = 1900

\*C = 1900

\*C = 1900

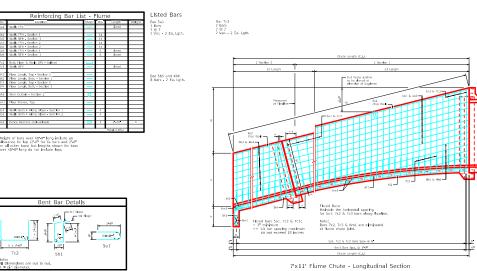
\*V = 988

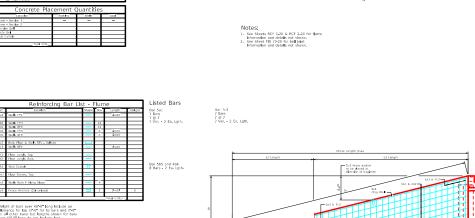
\*V = 988

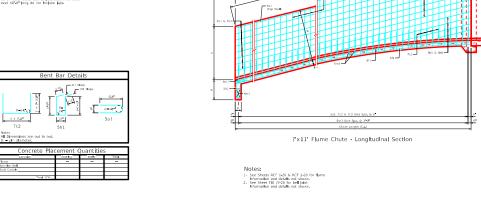
\*V = 988

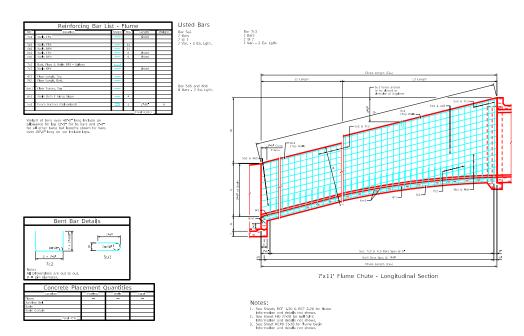
\*I = 180

\*C = 180





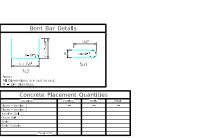


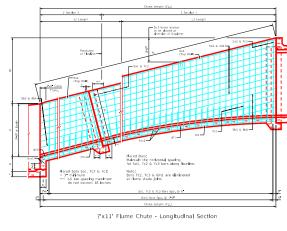


Bar 7c3 7 Bars 7 @ 7 7 Var. - 2 Ea. Lgth.



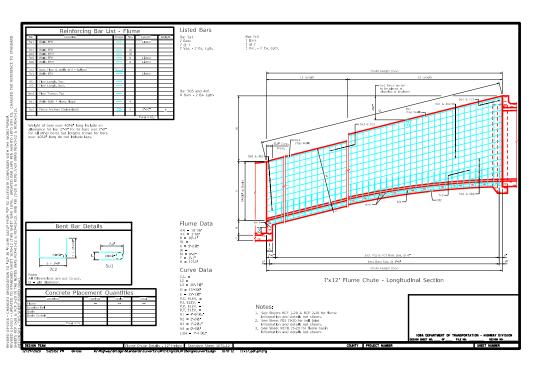


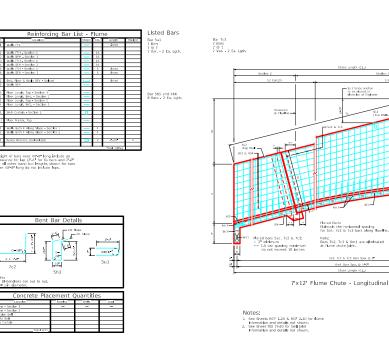


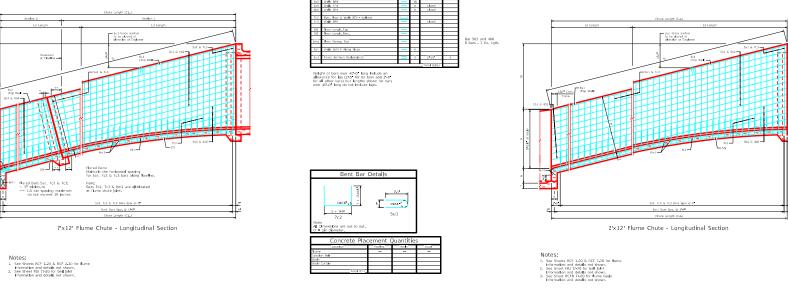


Notes: I. See Sheets RCF 1-20 & RCF 2-20 for fluinformation and details not shown. See Sheet FBI 32-20 for bellight Information and details not shown.





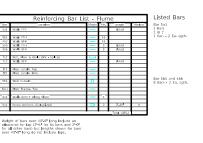


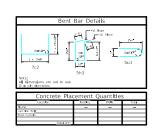


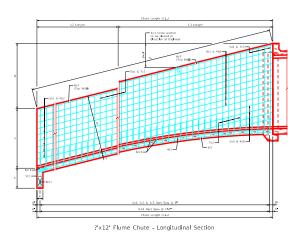
10 x 12	12 x 12	14 x 12	16 x 12
Flume Data  4A = 18'26' 4C = 1'00' 8 = 16'-1' SL = 2'' V = 0'-5'// W = 9'-0' T = 1'-1' H = 12'-0'	Flume Data  4A = 18726*  4C = 1700*  8 = 167.1*  SL = 57.4*  V = V-530*  W = 9-0*  T = 13.2*  H = 122-0*	Flume Data  4A = 18729  4C = 1700  8 = 18-17  SL = V = 9.5 %r  W = 9.07  T = 17-27  H = 122-07	Flume Data  4A = 18726  4C = 1700  B = 187-1  SL = V = V 5 %  W = V = V 5 %  T = 17.2  H = 1240
Curve Data	Curve Data	Curve Data	Curve Data
CL = 12 - 230 - 7X - 13 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130 - 130	CL = C. =	C.L. = 1.2 - 1.3 - 1.0 - 1.1 - 1.3 - 1.3 - 1.4 \text{\text{\$M\$}} \text{\$M\$} \	CL = C2 - C3 - C4

# 4:1 SLOPE FLUME

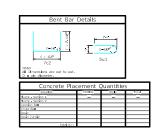
10 x 12	12 x 12	14 x 12	16 x 12
Flume Data  4A = 14*02* 4C = 1*00* 8 = 22*38* SL = V = 9*38' W = 9*0* T = 1*1* H = 12*0*	Flume Data  4A - 14'02'  4C = 1'00'  B - 22'-3K'  SL = '3K''  W - 9'-0  T - 1'-2'  H = 12'-0'	Flume Data  4A = 14/02' 4C = 1700' 8 = 22/38'' SL = V = V = 9/38'' W = 9/0' T = 17/2' H = 12/4''	Flume Data <a -="" 1'-2'="" 14'02'="" 22'-38'="" 9'-0'="" 9'-38'="" <c="1'00'" b="" h="12'-0'&lt;/td" sl="V" t="" w=""></a>
Curve Data	Curve Data	Curve Data	Curve Data
C.L. = 1.2 - 43.41%; 0 - 21.81%; 0 - 21.81%; 0 - 21.81%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71%; 0 - 21.71	C.L. = 13 - 4P-47K, 13 - 4P-47K, 10 - 27-87K, 10 - 27-97K, 10 - 27-97K	CL = 13 - 49 - 476,0 13 - 49 - 476,0 0 - 27 - 976,0 E - 27 - 776 P.C. ELEV - P.P. ELEV - P.P. ELEV - P.P. ELEV - P.T. ELEV - P.T. ELEV - P.T. ELEV - P.T. ELEV - T.T. 25 - 976, 32 - 25 - 976, 33 - 15 - 36,0 34 - 15 - 36,0 35 - 15 - 36,0 36 - 36,0 37 - 37 - 37,0 37 - 37 - 37,0 38 - 37 - 37 - 37 - 37,0 38 - 37 - 37 - 37 - 37 - 37 - 37 - 37 -	C.L. = 1.3 4.4 1/kg. 1.3 4.9 1.4 1/kg. 1.3 4.9 1.4 1/kg. 1.3 1.3 1.4 1/kg. 1.3 1.4 1.4 1/kg. 1.3 1.4 1.4 1/kg. 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.

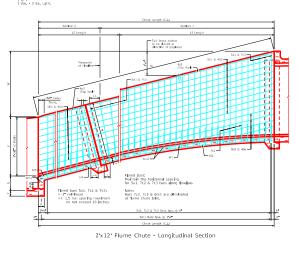


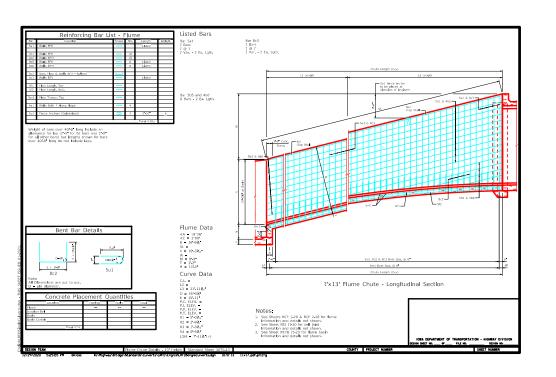


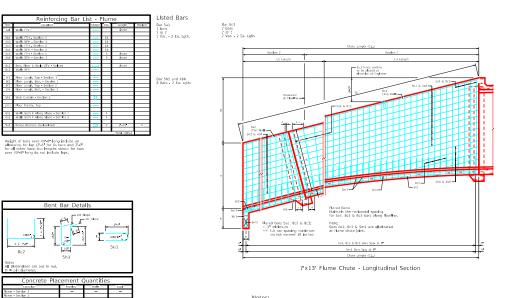


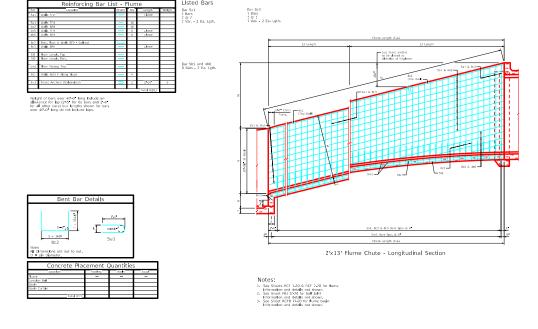












### 14 x 13 16 x 13

Flume Data	Flume Data
<a 18'26'<br="" ==""><c 1'00'<="" =="" td=""><td><a 18°26°<br="" ==""><c 1°00°<="" =="" td=""></c></a></td></c></a>	<a 18°26°<br="" ==""><c 1°00°<="" =="" td=""></c></a>
B 16 9K	8 16 9K
SL =	SI = 10.9%
V 10-3%	V 10 374
W = 10.37%	W = 10.37%
M 9 9	M = 9 9
T 1.2	T 1.2
H = 13.0"	H = 13.0"
Curve Data	Curve Data
Curve Data	Curve Data
C.L. =	C.L. =
L2 =	L2 =
L3 = 31 11N <sub>6</sub>	$L3 = 31.11 M_{\odot}$
D = 16 OK	D = 16 ON
E = 15 11	E = 15 -11
P.C. ELEV. =	P.C. ELEV. =
P.I. ELEV. = P.P. ELEV. =	P.I. ELEV. = P.P. ELEV. =
P.T. ELEV.	P.T. ELEV.
X1 5 0 X4	X1 5 0 Xs
X2 2 9 K	X2 2 9 K
X3 = 1 -3 N <sub>16</sub>	$X3 = 1 - 3N_4$
X4 = 0.3 K	x4 = 0.3 %
L3/4 7: 11% (+)	L3/4 7 112, (+)

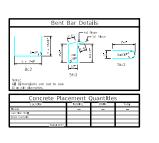
## 4:1 SLOPE FLUME

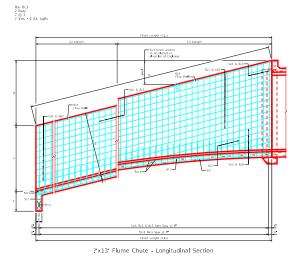
### 14 x 13 16 x 13

Flume Data	Flume Data
<a 14°02°<="" =="" td=""><td><a 14°02°<="" =="" td=""></a></td></a>	<a 14°02°<="" =="" td=""></a>
<c 1'00'<="" =="" td=""><td><c 1'00'<="" =="" td=""></c></td></c>	<c 1'00'<="" =="" td=""></c>
B = 22-3%	B = 22-3%
V = 10-0%	V 10 0%
W =	w =
M = 9-9 T = 1.7	M = 9-9 T = 1.7
H = 1350	H = 1330
Curve Data	Curve Data
C.L. =	C.L. =
L2 =	12 -
L3 45 4N <sub>6</sub> D 22 8M	L3 45 4 <b>X</b> <sub>1</sub> D 22 8 <b>X</b>
F 22 TK	D = 22.8% E = 22.7%
R.C. ELEV. =	P.C. FLEV
P.L ELEV	P.I. ELEV.
P.P. ELEV. = P.T. ELEV. =	P.P. ELEV. = P.T. ELEV. =
X1 5 3 M	X1 5 3M
X2 2 11W	X2 = 2 11 X
X3 = 1 3K	X3 = 1 -3 K
$X4 = 0.31 K_0$	X4 = 0'-31%,
L3/4 11 47 <sub>6</sub> ( )	L3/4 = 11 4 No ( )









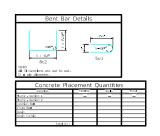
Notes

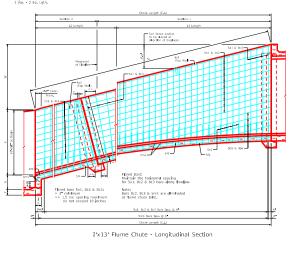
1. See Sheets RCF 1-20 & RCF 2-20 for flume information and details not shown.

2. See Sheet R6I 77-20 for bell joint information and details not shown.

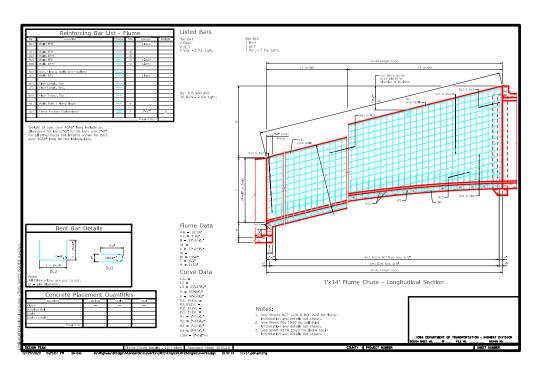


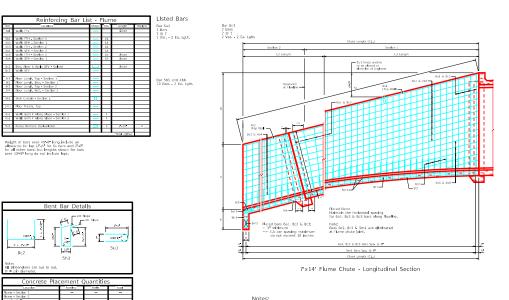
nce for lap (2.5° for 6s bars and 2.0° other bars) but lengths shown for bars (0.2° lang do not include large

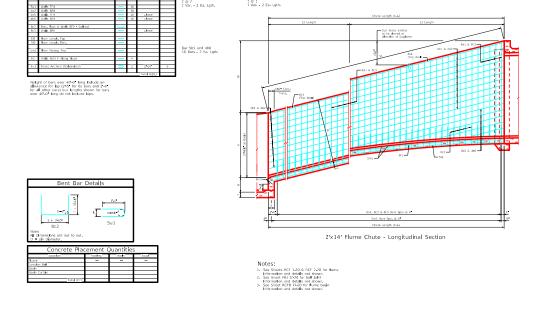




ee Sheets RCF 1-20 & RCF 2-20 for flume formation and details not shown. ee Sheet FBJ 77-20 for bell joint formation and details not shown. ee Sheet RCFB 77-20 for flume basin







### 14 x 14 16 x 14

Flume Data	Flume Data
<a 18'26'<br="" ==""><c 1'00'<="" =="" td=""><td><a 18*26*<br="" =="">≪C = 1*00*</a></td></c></a>	<a 18*26*<br="" =="">≪C = 1*00*</a>
B = 17 -51Ks	B = 17 5 17/6
SL = 11-0 <sup>3</sup> K <sub>2</sub>	SL = V = 11-0 <sup>1</sup> K <sub>2</sub>
W = M = 10-6	W = 10.6
T = 1 3	T = 1.3
H = 14-0"	H = 14.0"
Curve Data	Curve Data
C.L. = L2 =	C.L. = 12 =
L3 = 33 2 1/6	L3 = 33 2 1/16
D = 16 8N <sub>0</sub>	D = 16 8 N <sub>6</sub>
E 16 6 %; P.C. ELEV.	E 16 6 1/6" P.C. ELEV.
P.L. ELEV.	P.I. FLEV
P.P. ELEV. =	P.P. ELEV. =
P.T. ELEV.	P.T. ELEV.
X1 5 2 N <sub>0</sub>	X1 5 2 1/16
X2 2 11%	X2 = 2 -11V <sub>6</sub>
X3 1 3 1 X 1	$X3 = 1 \cdot 3^{1} X_{1}$
X4 0 31X <sub>11</sub>	$X4 = 0.3^{1}X_{0}$
L3/4 = 8 3X (-)	L3/4 = 8 3 X (-)

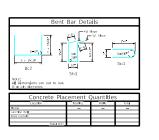
## 4:1 SLOPE FLUME

### 14 x 14 16 x 14

Flume Data	Flume Data
<a 14°02°<="" =="" td=""><td><a 14°02°<="" =="" td=""></a></td></a>	<a 14°02°<="" =="" td=""></a>
<c 1'00'<="" =="" td=""><td><c 1°00°<="" =="" td=""></c></td></c>	<c 1°00°<="" =="" td=""></c>
B = 24 -31 V <sub>14</sub>	B = 24 -31 V <sub>16</sub>
SL = V = 10-9%	SL = V = 10'-9%
V = 10 92	V 10.9%
M = 10 6	M = 10-6
T = 1 3	T = 113
H = 1450"	H = 14'+0"
Curve Data	Curve Data
C.L. =	C1 =
L2 -	L2 -
L3 47 3% <sub>6</sub>	L3 47 3 <b>7</b> <sub>11</sub>
D = 23 8N <sub>0</sub>	D 23 8V <sub>16</sub>
E = 23 7 No	E = 23 7 Vic
P.C. ELEV. = P.I. FLEV. =	P.C. ELEV.
P.P. FLEV	P.P. ELEV.
P.T. ELEV	P.T. ELEV
X1 = 5 -5%	X1 = 5.5%
X2 = 3-1	X2 3 1
X3 = 1-4V <sub>6</sub>	X3 = 1 + N <sub>6</sub>
X4 = 0-4K*	×4 = 0 -4%
L3/4 = 11 9% (+)	L3/4 = 11 9½ (+)



eight of bars over 40.0 Tong Include an lowence for lap (2.5 for 6s bars and 2.0 r all other bars) but lengths shown for bars er 40.0 Tong do not include laps





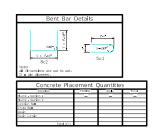
Notes

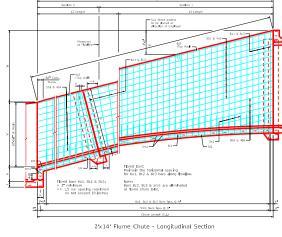
1. See Sheets RCF 1-20 & RCF 2-20 for flume information and details not shown.

2. See Sheet R6I 77-20 for bell joint information and details not shown.



ance for lap (2.5° for 6s bars and 2.0° I other bars) but lengths shown for bars





CES: te Sheets RCF 1-20 & RCF 2-20 for flume formation and details not shown se Sheet FBJ 77-20 for bell joint

